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ATMOSPHERIC ENVIRONMENT FOR SPACE SHUTTLE (STS-5) LAUNCH

By D. L. Johnson, C. K. Hill, and G. W. Batts Space Science Laboratory

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This report presents a summary of selected atmospheric conditions observed near Space Shuttle STS-5 launch time on November 11, 1982, at Kennedy Space Center, Florida. Values of ambient pressure, temperature, moisture, ground winds, visual observations (cloud), and winds aloft are included. The sequence of preiaunch Jimsphere measured vertical wind profiles is given in this report. Also presented are the wind and thermodynamic parameters measured at the surface and aloft in the SRB descent/impact ocean area. Final meteorological tapes, which consist of wind and thermodynamic parameters versus altitude, for STS-5 vehicle ascent and SRB descent have been constructed. The STS-5 ascent meteorological data tape has been constructed by Marshall Space Flight Center in response to Shuttle task agreement No. 936-53-22-368 with Johnson Space Center.

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TECHNICAL MEMORANDUM

ATMOSPHERIC ENVIRONMENT FOR SPACE SHUTTLE (STS-5) LAUNCH

I. INTRODUCTION

This report presents an evaluation of the atmospheric environmental data taken during the launch of the Space Shuttle/STS-5 vehicle. This Space Shuttle vehicle was launched from Pad 39A at Kennedy Space Center (KSC), Florida, on a bearing of 90 deg east of north at 1219 UT (0719 EST) on November 11, 1982.

This report presents a summary of the atmospheric environment at launch time (L+0) of the STS-5, together with the sequence of prelaunch Jimsphere measured winds aloft profiles from L-14 hr through liftoff. The general weather situation for the launch and flight area is described, and surface and upper level wind/thermodynamic observations near launch time are given. Surface and upper level wind/thermodynamic parameter measurements are also presented for the SRB descent/impact analyses.

Previous MSFC-related launch vehicle atmospheric environmental conditions have been published as Appendix A of individual MSFC Saturn Flight Evaluation Working Group reports [1]. Office memorandums have been issued for previous flights giving launch pad wind information. A report has also been published [2] which summarizes most launch atmospheric conditions observed for the past 155 MSFC/ABMA-related vehicle launches through SA-208 (Skylab 4). Reports summarizing ASTP, STS-1, STS-2, STS-3, and STS-4 launch conditions are presented in References 3, 4, 5, 6, and 7, respectively.

II. SOURCES OF DATA

Atmospheric observational data used in this report were taken from synoptic maps made by the National Weather Service, plus all available surface observations and measurements from around the launch area. Upper air observations were taken from balloon-released instruments sent aloft from Cape Canaveral Air Force Station (CCAFS) and from the ship Gen. H. S. Vandenberg in the Atlantic Ocean off the Florida coast. High-altitude winds and thermodynamic data were measured by the Super-Loki rocketsondes launched from the CCAFS. Table 1 presents a listing of systems used to obtain the upper level wind profiles used in compiling the final ascent meteorological data tape. Only the ship-launched Omegasonde-Rawinsonde and Super-Loki rocket data were used in the upper level atmospheric regions for the construction of the final SRB descent/impact meteorological data tape. Data cutoff altitudes are also given in Table 1.

III. GENERAL SYNOPTIC SITUATION AT LAUNCH TIME

A ridge of high pressure, located off the northeast Atlantic coast, and extending through southern Alabama into the Gulf of Mexico, was an atmospheric influence over the Florida peninsula during the early morning launch. Along the peninsula, surface winds were northeasterly to easterly, ranging in magnitude

from 10 to 17 ft/sec. Very little cloud cover was present, along with low humidity and warm temperatures (low 70's) prevailing throughout the early morning countdown period. Figure 1 gives the surface weather map 19 min prior to launch. Figure 2 presents the wind flow aloft at the 500 mb level. Northwesterly winds dominated the flow aloft over the KSC Florida area.

Cloudiness was not very prevalent over the Florida peninsula or the KSC launch complex as shown in Figure 3. Figure 3 presents the GOES-5 visible picture taken 41 min after launch (1300 UT). Scattered cumulus clouds at 1200 ft were present during launch. Figure 4 shows an up-close visible shot of the Florida peninsula as recorded by GOES-5, taken at 1300 UT.

IV. SURFACE OBSERVATIONS AT LAUNCH TIME

Surface observations at launch time for selected KSC locations are given in Table 2. Included are pad 39A, Shuttle runway, and CCAFS balloon release station observations. Neither precipitation nor lightning was observed at launch time.

Table 3 presents Pad 39A wind data along with other standard hourly meteorological measurements and sky observations for the 6-hr period prior to launch of STS-5. Values for wind speed and direction are given for the 84 m (275 ft) FSS reference level and 18 m (60 ft) pad light pole level.

V. UPPER AIR MEASUREMENTS DURING LAUNCH

The FPS-16 Jimsphere (1235 UT), MSS rawinsonde (1348 UT), Super-Loki rocketsonde (1605 UT), and Super-Loki Robin (1445 UT) systems were used to measure the upper level wind and thermodynamic parameters for STS-5 launch. At altitudes above the rocket-measured data, the Global Reference Atmosphere (GRA) [8] parameters for November KSC conditions were used. A tabulation of the STS-5 final meteorological data for ascent is presented in Table 4 which lists the wind and thermodynamic parameters versus altitude. A brief summary of parameters is given in the following paragraphs.

A. Wind Speed

At launch time, wind speeds were 22.0 ft/sec (3.4 kn) at 60 ft and increased to a maximum of 146 ft/sec (86 kn) blowing from 336 deg. This maximum occurred at an altitude of 40,600 ft (12,375 m). The winds decreased above this level and then became stronger again at much higher levels, as shown in Figure 5. The overall maximum measured speed was 271 ft/sec (160 kn) at 185,000 ft (56,388 m) altitude.

B. Wind Direction

At launch time, the 60-ft wird direction was from the east (90 deg) and shifted through the north to a northwesterly component above 18,000 ft (5486 m). The winds then shifted into the winterwesterly regime above 86,000 ft (26,213 m). Figure 5 shows the complete wind direction versus altitude profile. As shown in Figure 5, wind directions became quite variable at altitudes with low wind speeds.

C. Prelaunch/Launch Wind Profiles

Prelaunch/launch wind profiles presented in Figures 6 through 9 were measured by the Jimsphere FPS-16 system. Data are shown for five measurement periods beginning at L-14 hr and extending through L+0.

The wind speed and direction profiles for the 14-hr period prior to and including L+0 are shown in Figures 6 and 7. The in-plane (right crosswind) and out-of-plane (left crosswind) profiles are given on Figures 8 and 9. The wind speeds were significantly greater than the November mean values in the 30,000 to 40,000 ft layer. Also, unusually strong northerly winds persisted during the 14 hr prior to L+0. Consequently, the peak measured wind speed at L+0 of about 150 ft/sec from a NNW direction at approximately 40,000 ft produced a left crosswind component of approximately 135 ft/sec. This equaled the 99th percentile statistical value obtained from November climatological records. A more detailed summary of the atmospheric patterns influencing STS 5 is presented in Appendix A of this document.

D. Thermodynamic Data

The thermodynamic data taken at STS-5 launch time, consisting of atmospheric temperature, dew-point temperature, pressure, and density have been compiled as the STS-5 ascent meteorological data and are presented in Table 4. The associated thermodynamic data taken in support of the SRB descent have also been assembled as the STS-5 SRB descent/impact meteorological data and are presented in Table 5. The vertical structure of temperature for the STS-5 ascent and for the SRB descent is shown graphically versus altitude in Figure 10.

The atmospheric thermodynamic parameters of temperature, pressure, and density, measured during STS-5 launch below 120,000 ft, were generally within 5 percent of their respective PRA-63 [9] annual values. All these parameters stayed within 20 percent of their respective PRA-63 values, at all levels.

E. SRB Upper Air and Surface Measurements

As has been mentioned in earlier paragraphs, an SRB descent meteorological data tape has also been constructed which consists of data taken from the Omegasonde-Rawinsonde system (1250 UT) aboard the USNS Vandenberg, which was stationed off the coast in the Atlantic Ocean. The CCAFS measured Super-Loki rocketsonde data and the GRA model data were used at altitude levels above the measured Omegasonde data. The tabular values for the SRB descent meteorological tape are presented in Table 5, with wind speed and direction profiles presented in Figure 11. Figure 10 gives the vertical temperature profile.

The surface-ship me eorological and oceanographic observations taken close to STS-5 SRB impact are presented in Table 6.

VI. ATMOSPHERIC SUMMARY CONDITIONS FOR STS LAUNCHES

Given in Table 7 are selected atmospheric I+0 launch conditions for all the Space Shuttle launches.

TABLE 1. SYSTEMS USED TO MEASURE UPPER AIR WIND DATA FOR STS-5 ASCENT*

The left of the le

	Date: Novemb	November 11, 1982		Portion of Data Used	ata Used	
	Release Time	Time	Start		End	
Type of Data	Time (UT) (hr:min)	Time After T+0 (min)	Altitude m (ft)	Time After T+0 (min)	Altitude m (ft)	Time After T+0 (min)
FPS-16 Jimsphere	12:35	91	6 (21)	16	17,069 (56,000)	74
MSS Rawinsonde	13:48	86	17,374 (57,000)	146	28, 042 (92,000)	181
Super-Loki Rocketsonde (Datasonde)	16:05	226	68,885 (226,000)	226	28,346 (93,000)	248
Super-Loki Rocketsonde (Robin)	14:45	146	84,430 (277,000)	146	69,190 (227,000)	147
Omegasonde-Rawinsonde*	12:50	31	18 (60)	31	28,042 (92,000)	123

*The Omegasonde-Rawinsonde was released from the USNS Gen. H. S. Vandenberg to measure the upper atmosphere for SRB descent/impact analyses.

TABLE 2. SURFACE OBSERVATIONS AT STS-5 LAUNCH TIME

								Sky Cover		3	Wind
Location ^a	Time Afrat L+0 (mun)	Pressure (MSL) N/cm ² (psia)	Temperature °K (°F)	Dew Point °K (°F)	Relative Humidity (%)	Visibility km (miles)	Cloud** Amount (Tenths)	Cloud Type	Height of Base Meters (ft)	Speed ft/sec (kt)	Direction (deg)
NASA Space Shuttle Runway ^e Winds Measured at 10.4 m (34 ft)	0	10.233 (14.842)	295.4 (72.0)	291.0	75	16 (10)	-	Strato- Cumulus	1219 (4,000)	8.4 (5.0)	080
Surface Measurements	0	10.227 (14.833)	294.9	290.4 (63.0)	92	16 (01)	-	Strato- Cumulus	975 (3200)	15.2 (9.0)	060
Pad 39A Lightpole ^d SE 18.3 m (60.0 ft)	0	10.227* (14.833)	295.2 (71.6)	286.7 (56.4)	65	ľ	I	١	ı	22.0 ^b (13.0)	_q 06
Pad 39A FSS (Top-SE) 83.8 m (275 ft)	0	ı	ı	_	l	ł	1	-	ı	35.0 ^b (20.7)	\$

• Pad 39A Camera Site 3 barometric pressure instrument appeared to be reading too low. Therefore, the KSC Shuttle runway station pressure value interpolated to 10,227 N/cm² at 21 ft above MSL would be more appropriate as the L+0 pad atmospheric pressure measurement.

•• One-tenth total sky cover.

a. Altitudes of measurements are above natural grade, except where noted.

b. Approximately I min average prior to L+0.

c. Balloon release site.

d. Pad 39A thermodynamic measurements are taken at camera site No. 3, approximately 6.4 m (21 ft) above MSL.

e. Official STS-5 sky observational site.

TABLE 3. STS-5 PRE-LAUNCH THROUGH LAUNCH KSC PAD 39A METEOROLOGICAL MEASUREMENTS*

mber 1982 Temp. Point RH (SE)** (SE)** ne UT (°F) (°F) (%) WS Kt WD (SE)** 0700 71 61 70 23 080 11 080 2 0800 70 59 68 23 090 9 090 1000 71 59 67 22 090 12 090 1100 71 55 62 23 090 13 090 1100 71 55 64 22 080 13 090	Hourly Atmospheric Me	spheric M	easurement _s	t;			Sky	Sky Condition	E	
moer 1982 1 emp. Font of (F) (R) WS Kt WD WS Kt WD 0700 71 61 70 23 080 11 080 2 0800 70 59 68 23 090 9 090 0900 71 59 67 22 090 12 090 11000 71 57 62 23 090 12 090 11000 71 55 58 22 090 13 090 1200 71 58 64 22 080 13 080	E		275' I (SE.	Level	60° Le (SE)	evel		Total	Vic	e H
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1200 71 58 64 22 080 13 080	7.1		22	060	13	060	1/10 SC at 4,000 ft	1/10	10	
	71		22	080	13	080	1/10 SC at 4,000 ft	1/10	01	
61 68 21 090 13 090	72 61		21	060	13	060	1/10 SC at 4,000 ft	1/10	10	

Hourly observations obtained verbally from CCAFS.

** 10 min mean about the hour from pad 39A instrumentation.

*** L+0 PAD Wind and thermodynamic parameters obtained from HOSC strip cuarts. SE Anemometers used at 60 and 275 ft levels for L+0 wir. Leonditions (approximately 1 min average prior to L+0). Pad 39A L+0 atmospheric pressure, at 21 ft (MSL), was 10.227 N/cm². Sea level pressure was 10.233 N/cm².

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001900	0.33	B.7	0.01	.8229+D3			2.4
006200	0.35	9 0	0.0	10+618	1006+04		
006300	0.39	040		8149+03			•
004900	031	7.60	6-6	PO+0P167	FC+ 1000		•
004500	o To	019	7.0		•		•
009900	0.15	1 40	4		00000		. :
004700					FO - FO - FO	(.
004900	900	· · · · · · · · · · · · · · · · · · ·	6.	70,000			•
	9 e e	C 4	•	1011708		. > 4	7.1
20000	970		P	50+166	**************************************	~ 1	1:1:
00000	770	25	m (. 7962+03	ر ک	ĸ:	-2.2
001700	777		2.6	. 1933+03	.9764+03	V.	-3.4
002/00	017	05.1	6.5	.7904+03	.9732+03	3	9.4-
D07300	017	D4 5	9.1	. 7875+03	-9699+03	ŗ	-5.1
007400	710	053	0.1	.7846+03	.9667+03	ר אני 10	7.0
005200	916	D#1	0.6	7617+03	.9635+03	G	-4.2
001600	013	101	0.6	.7789+03	.9602+03	i E L	
007700	013	₩ 60	0.6	. 1760+03	.9570+03	e III	9.0
00100	019	O90	6.0	.7732+03	.9538+03	7 3 Y	9.1
004200	019		6°8	.7703+03	.9506+03	7	3.0
000000	610	11.2	8.8	.7675+03	.9473+03	7	4.2
DOALDO	0.18	101	0.6	.7647+03	.9432+03	ř	-14.0
008200	710	105	9.2	.7619+03	-9391+03	-13	3.9
008300	013	109	8.6	-7591+03	.9351+03	1-	3.7
004800	900	980	9.6	.7563+07	.9310+03	-	3.6
008 800	900	06 4	9.7	.7536+03	, 9269+03	-13	
009800	400	**6	6.6	.7508+03	.9229+03	-13	3.3
002800	200	01.1	10.1	.7491+03	.9189+03	-13	3.1
008800	600	01 1	10.3	.7453+03	.9149+03	-13	3.0
008900	900	019	10.5	.7426+0;	.9109+03	-1	2.9
00600	900	7 00	10.7	.7399+03	.9070+03	7-	2.7
001600	600	600	10.5	.7372+03	.9042+03	-12	2.6
002600	800	028	10.4	.7345+03		7	2.9
006630	900	027	10.2	.7318+03	.8987+03	-12	2.9
004600	600	800	10.0	.7291+03	.8960+03	-13	3.0
003600	ato.	010	6.6	.7265+03	.8932+n3	7	3.1
009600	800	0.2.7	9.1	.7238+03	٠	7	3.2
- L01600		35.7	20.00	-	.8878+03	-	M .
009800	010	- 65					
				20+5K12-			,

ALTITUDE	WIND SPEED	WIND DIRECTION		PRESSURE	DENSITY	6	DEW POINT
161)		1066)	(056,0)	(MILLIBARS)	(GRAM/H3)		10 5301
000010		35.5	0.6		.8796+03		-13.5
01010	013	15.A	9.9	.7106+03	.8772+03		-13.8
010200	012	010	80 ° 00	.7080+03	.8747+03		-14.0
010300	110	500	m • 6	.7054+03	.8722+03		-14.3
010400	# (C)	003	O •	.7028+03	.8698+03		-14.5
010500		· · · · · · 600 · · · · ·	7.6	٠	.8673+03		8.7[-
010600	0.15	910	7.6	•	.8649+03		-15.1
010200	0.10	210	Z	•	.8625+03		-15.3
010800	017	# ! (O	7.1	•	.8600+03		-15.6
010900	910		10 ·	* 6900+03	.8576+U3		-15.6
01110	910	920	0 :	•	£0+255 8 *		1.91-
			•	٠	50-97CB-		- 10.5
011200	610	120	N• •	.68234U3	.8500+03		100
204110	710	034	0	8 8			9.91
011500	910	120		. <u> </u>	8.22+01		-16.0
011600	021	035			8396+03	(-17.1
011700	-019		M • 10	416	.8371+03	OR OF	-17.3
011800	020	037	5.2	.6673+03	.8345+03	iC I	-17.5
011900	0.24	041	0.4	.6648+03	.8319+03) -	-17.6
012000	0.25	04.2	0. 1	.6623+03	.8294+03	4 <i>F</i>	-17.8
012100	021		9. 1	.6598+03	.8268+03	IL R	-17.4
012200	022	031	\$ • *	.6574+03		F	-17.0
012300	0.22	03.8	M.	. 6549+03	.8215+03	م کال	-16.6
012400	910	036	N (• 6528+03	.8189+03	C) JA	-16.2
012500	0.18		D • #	9	.8162+03	I Li	-15.8
012600	610	020	40 f	.6476+03	.8136+03	iT	-15.4
012700	910	000	~ v	•	.0.10.03		9.61
01280) W	n 4	5 D+82 F9+			
)	7 4 6	7 (°				
013100	0.20		70 1	.0.0000	.0.1000		8 M -
013200	023	6 00	2.00	-6332+03	.7981+03		-13.9
013300	021	056	2.7	.6308+03	.7955+03		-13.9
013400	022	n5.7	2.6	.6285+03	.7930+03		-13.9
013500	025	₩ 90	2.4	.6261+03	.7904+03		-13.9
013600	024	0 6 S	2.3	÷	.7879+03		-14.0
013700	025	055	2.5	£0+140°	.7854+03		-14.0
	750	*****	0.7	•	50.000.		3.
	0.28	, see 0	10 fr	.01684US	.7803+03		
			- 0		CO. D. / L.		
014200	027	. vs.	200	•	.7733+03		
014100	020	200			7711+01		7.41-
014400	020	038		•	.7688+03		-14.8
014500		036	.	.6029+03	.7666+03		-14.9
014600	030	031	1 M	.6006+01	.7644+03		-15.1
014780	0.29	034	•	.59A4+DT	.7522+03		-15.3
_	620	52.7	2	.5941+03	.7600+03		-15.5
	0.72	02.8	٠	.5939+03	.7578+03		-15.6

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(FT)	(FT/SEC)	10 10 10 10 10 10 10 10 10 10 10 10 10 1			UEMS I I I	DE W	104
Attent		1990	ייי נמנפ כו	(WILLIBARS)	(CEVIXA)	301	5
01510	0.52	0.00	r	.5916+03	.7556+03		-15.
015200	47.0	23.1		10+868°	.7529+03		-16.
01210	7 6	2	10 (5D+1/B5•	N		-16.
01540	7	170	6.	•	٠		-17.
00000	900	9 10	6. -	.5827+03	.7449+03		-17
000010		010	-1.0	.5804+03	.7423+03		-17.
00000	0.35	610	-1-1	.5782+03	.7396+03		-16.
201610	11.58	0.18	-1.1-		.7370+03		-16.
000010		120	-1.2	.5738+03	.7344+03		-19.
	0.36	210	-1.2	.5717+03	.7318+03		-19.
000910	010	013	-1-3	.5695+03	.7292+03		-20-
016100	037		-1-4	.5673+03	.7267+03		-20-
016200	039	\$ 0 0	-1.5	.5652+03	.7241+03		-20-
016300	0.00	010		5630+03	.7216+03		-20
016400	0.39	700	-1.7	.5609+03	.7191+03		-21.
016500	043	00 7	-1.07	5587+03	.7166+03		-2
016600	045	600		5566+03	7161404		-21
016700	DAS		-1-0		7117401		22
016800	8# C	200	-2-0	10.42.42	**************************************		,
016900	048	00.5	-2.1	1000 F 10	1041404		227
017000	0.50	36.0		10. 10.00 ;	2048404		111
017100	0.87	15.6	-2.2	100 Tare	1001000		,,,
017200	9,0	35.6	F 6-	10+0445°	10007		
017300	0.50	356	7 - 6		10 - 16 - 10 - 10 - 10 - 10 - 10 - 10 -		
017400	840	353	C - C -	. 5.40 P. C.			
017500	DAR	152	7 . 6 . 1	- CO. CO. CO.	1001740		
017600	940	35.1	2.6	101010101 101010101	1001019	.	-23
017700	0.45	350	2.5-		NC + 1 + 0 + 1		
017800	**0	36.7	9-6-	10000000000000000000000000000000000000	5040000°		
017900	DAI	345	-2-6	E 2010	10.11.00.		* * *
018000	940	9 42	-2-7		071+070P+		
Olston	0.93	40 M	-22.0	20.00 TO	50.24.00		
018200	## C	13.9		10.0170.	10 + 0 + 1 + 1 + 1 + 1 + 1 + 1 + 1 + 1 +		
01.300	043	625	1 pr	٠.	10000000000000000000000000000000000000		
010400	0.38	116	1 46 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	CO-0170.	£0.8219.	•	-67-
018500	480	400) 4 		FD-1019-		•
018600	039	13.7) es) r) r	٠.			
018700	0.37	2 1 2	0 0	F049E49	100000		•
018800	037	111	0 C	******	**************************************		- 20
014900	35.0	4 PM	7 4 1	FO + 9 1 1 C •			•
01900	033	333	7 42 1	-0.000 -0.000 -0.000	4 B 0 U 3 4 U 3		971
019100	110	111	9 0		50.7050		•
019200	031	777	\		20.0000		-26.
019300	25.0	* **		: D - J : D - S	50+5464		-76.
010400	0.40	C 45	r f	.5018+03	50-92C9*		-27.
019400	0 e	245		50+866#.	* 6508+03	•	-27.
	920	0 · 4) · ·	80+6/6#•	•	•	-21.
000010	620	1 #5	-6.3	.4960+03	.6471+03	•	-27.
007610	030	34.7	-6.6	**9*O*O3	.6453+03		-27.
008410	620	346	-6.8	.4921+03	•6435+03	•	-27.

ALTITUDE	WIND SPEED	WIND DIRECTION	TEMPERATURE	PATSSUPE	DEMSITY	A 3Q	POINT
IFT)	(F1/SEC).	19301	(066 C)	(MILLIBARS)	(GRAM/R3)	=	1066 C1
020000	030	34.0	-7.4	.4883+03	.6398+03		-27.8
020100	021	38.2		4864+03	.6380+03		-27.9
02020	031	34.5	0.6-	80+9808°	.6362+03		-26.1
020300	D28	349	-8-2	.4826+03	.6144+03		-28.2
020400	029	346	-8.5	.4607+03			-28.4
020500	030	319	9-9-	.4788-03	.6307+03		-28.5
02000	0.28	34.8	-9+1	.4770+03	.6289+03		-28.7
020200	028	315	: 4.6-	. 4751+03	.6271+03		-28.8
02000	0 2 8	350	9.6.		*6254+03		-29.0
006020		348	6.6-	.4714+03	•6236+03		-29.1
000120	620	# #M	-10.2	.4695+03	.6218+03		-29.3
021100	920	348.	-10.5	.4677+03	.6200+03		-29.4
02120	0.26	0 m	О.	•	№.		-29.5
Uctour	0.28	240	0.11.	**************************************	.6164.03		-24.5
021400	027	M Pin	-11-3	22.	.6146+03		-29.6
021500	926	- 3433	9-11-	m :	.6129+03		-29.7
021600	0.20 0.00	15 to	6-11-	ND+S08+	.6111+03		-29.8
021700	027	338	-12-2	- 4567+D3	.6093+03	(-29.9
071400	200	N 10 10 10 10 10 10 10 10 10 10 10 10 10	15.4		.6076+03	OR OF	-29.9
022000	0.20	116	0.51		100100	10 F	
022100	0.50	110) F	10.00 M	10.1.00.	:11 >C	
02220	0.30	133	9 4 9 M	10 - 11 - 11 - 11 - 11 - 11 - 11 - 11 -	6065-03	\{} ()O	7.07
022300	D28			NO+6844	.5987+03	L R	-30.2
022400	0.32	32.6	-14.0	NO+11444	.5969+03	F	-30.2
022500	<u>0</u> 32	329		.4424+03	.5951+03	ን ያ ኒ	-30.2
022600	031	32.5	-14.6	.4406.03	.5933+03	G A	-30.3
022700	033.	321	-14.0	.4366+03	.5915+03	i Li	-30,3
022800	033	32.4	-15.1	.4371+03	.5898+03	is T	-30.3
022900		320	-15-3	.4353+03	.5880+03	5 Y	- 30 • 4
023000	0.36	51 O	15.6	10+9164·	.5862+03		- 30.4
001520		320		**************************************	.5844+03		- 30 - 3
02220		31.0	<u>.</u>	5	.5826+03		- 30 - 2
005550	770	21 A 11 A	5.41-	10++87F	204403		- X
023500		315		FC+9404	5777403		130.0
023600	**0	31.2	-17-1	4232+03	.5755+03		-29.9
023700	DAB	312	-17.3	-4215+03	.5738+03		-29.8
023800	0 *7	316	-17.6	10-8614	.5720+03		-29.1
023900	1011	31.4	-17.8	.4181+03	.5702+03		-29.6
000,50	0.50	31 3 -	-16.1		.5685+03		-29.5
024100	020	S (M)	-	.4147+03	.5666+03		-29.7
054500	150	31.4 31.4	60 - C	-4130+03	.5647+03		-30-0
024450	054	314	<u> </u>	113	.5628+03		- 30.2
004400	* CD	118	= -	50.400	.5609+03		-30.5
007460	150	# N	0.61	. 4040+03	.5590+03		7.R-
		515 515 516	2-61-		.5571+03		# :
001770	200	2.10	- C	0 - / - 0	7		5.15-
200420	200	116	n	ED+050+	50.0566		6161
•	***	,	b	-	\$0.clec•		1115

00000000000000000000000000000000000000	325030	(F.7/SEC)					
ORIGINAL PAGE IS OF POOR QUALITY OF POO			105.61	LOSSATURE	PRESSURE	1	
ORIGINAL PAGE (5 OF POOR QUALITY ORIGIN	02512) (31.8	ِ ب	(MILIBARS)	ALT SHOOT	
ORIGINAL PAGE IS OPPOR QUALITY ORIGINAL PAGE IS OPPOR QUALITY	025200	300	118	6.61	-	CHARAS.	
ORIGINAL PACE IS OF POOR QUALITY ORIGIN	025300	87 D	319		:	50+645·	- 12.0
ORIGINAL PAGE (5 OF POOR QUALITY COLOR 10 OF P	25400	8,0	16	-50.5		.5477+03	4 62
ORIGINAL PAGE IS OF POOR QUALITY ORIGIN	25500	910	12.5	20.3		.5458+03	,
ORIGINAL PAGE 15 10 10 10 10 10 10 10 10 10 10 10 10 10	25400	0.45	13.6	-20.4	50,4445	.5438+03	4.36
ORIGINAL PAGE 13 ORIGINAL PAGE 13 ORIGINAL PAGE 13 OF POOR QUALITY ORIGINAL PAGE 13 OF POOR QUALITY ORIGINAL PAGE 13 ORIGINAL PAGE 13 OF POOR QUALITY ORIGINAL PAGE 13 ORIGINAL PAGE 1	26.75	S*0	23		50+5545	.5419+03	2001
ORIGINAL PAGE (5) ORIGINAL PAGE (5) OF POOR QUALITY ORIGINAL PAGE (5) OF POOR QUALITY ORIGINAL PAGE (5) ORIGINAL PAGE (5)	100000	040	926	-20.7	10+01A5+	.5400+03	1.55-
ORIGINAL PAGE 132 1111 1111 1111 1111 1111 1111 1111	25000	**0	97	-20.8	3,	.5380+03	1.000-
ORIGINAL PAGE (5) OF POOR QUALITY ORIGINAL PAGE (5) ORIG	מחאבי	0.02	926	-20.0	200	.5361+03	9.00
ORIGINAL PAGE 131 191 191 191 191 191 191 191 191 191	2000	740		1.12	3		-38.0
ORIGINAL PAGE 173 173 173 173 173 173 173 173 173 173	26100		333	1017	ž		-35.4
ORIGINAL PAGE 111 111 111 111 111 111 111 111 111 1	26200	240		7.12	-3837+03	5005265	-35.9
ORIGINAL PAGE 1111 112 112 1130 1130 1130 1130 1130 1	26.300		33.7	h-12	• 3821+0T	ED+ ans c ·	1.96-
ORIGINAL PACE 22.7 171. 172. 172. 172. 172. 172. 172.	00492	0.00	300	-21.7	. 3805+02	.5287+03	7-71-
ORIGINAL PAGE 52.5 1117-01 1010 0010 0010 0011 1010 0010 0	6500	240	34.1	21.9	.3790+01	.5270+03	4.41-
ORIGINAL PAGE 13 OF POOR QUARTY ORIGINAL PAGE 13 ORIGINAL	26600	100	33.8	-22.2	.3774+01	£0+4526+	-37.1
ORIGINAL PAGE 1314 1915 1915 1915 1915 1915 1915 1915 19	26.700	**0	740	22.4	2769404	.5237+03	4 62 1
ORIGINAL PAGE 13. 1767 - 22. 1768 - 1	24000	100		-22.6	70.66.66	-5221+03	
DRIGINAL PAGE 1915 1915 1915 1915 1915 1915 1915 191	0000	I * 0	645		2010101	(7
Day 188	1000	DAG	2 * 4 *	-23.1	50.42/5.	01	
GINAL PAGE: 10.000	0002	041		23.4	50+12+03	171+03	
NAT	2007	043	34.5	-23.6		55.03	
181	007	0.45		-21.A	• 5682+03	O	
Description 1885	7300	Des	34.5	-24-1		0	7
Description	00	043		-24.1	. 3651+03	R	
Colored Colo	0000	900		-24.5	. 3636+03	ζ	
0 0	009	0.03		7.42	• 3621+03)U	
Column	700	240		-25.0	3606+03	A	
047 346 -25.7 -3546+03 -5023+03 -5010+03 -5010+03 -5010+03 -5010+03 -5010+03 -5010+03 -5010+03 -5010+03 -5010+03 -5010+03 -5010+03 -5010+03 -5010+03 -5010+03 -5010+03 -5010+03 -5010+03 -5010+03 -5010+03 -6010+03	800	940		25.2	-3591+03	LI	
047 346 -25.7 -3564-03 -507-03 -6.0 046 346 -25.9 -3546-03 -4075-0	006		346	1-20-	-3576+03	T	
0 % 3 % -25.9 -35%6.03 -9991.03 0 % 3 % -26.7 -35%6.03 -4975.03 0 % 3 % -26.7 -35%1.03 -4975.03 0 % 3 % -26.7 -35%1.03 -4975.03 0 % 3 % -26.7 -26.7 -49%3.03 0 % 3 % -27.2 -34%1.03 -49%3.03 0 % 3 % -27.2 -34%1.03 -49%2.03 0 % 3 % -27.2 -34%1.03 -49%2.03 0 % 3 % -27.2 -34%1.03 -49%6.03 0 % 3 % -27.7 -34%2.03 -49%6.03 0 % 3 % -27.7 -34%2.03 -49%6.03 0 % 3 % -27.7 -34%2.03 -48%6.03 0 % 3 % -28.7 -34%1.03 -48%6.03 0 % 3 % -28.7 -34%6.03 -48%6.03 0 % 3 % -28.7 -28.7 -28.7	000	047	34.7	F. 36-	.3561+03	Y	
046 348 -26.2 -3531-03 -4975-03 048 348 -26.7 -3517-03 -4959-03 048 350 -26.7 -3487-03 -4959-03 051 349 -27.2 -3487-03 -4959-03 051 349 -27.2 -3487-03 -4959-03 052 352 -27.2 -3487-03 -4997-03 053 352 -27.2 -3481-03 -4997-03 054 352 -27.7 -3429-03 -4997-03 056 353 -27.2 -3490-03 -4891-03 056 352 -28.2 -3490-03 -4831-03 057 352 -28.2 -3340-03 -4816-03 059 352 -28.2 -28.3 -3400-03 -4816-03 059 350 -28.2 -28.5 -337-03 -4816-03 -475-03 059 350 -29.2 -334-03 -475-03 -475-03 059 350 </td <td>100</td> <td>-</td> <td>346</td> <td>125.0</td> <td>.3546+03</td> <td>200000</td> <td>-40.7</td>	100	-	346	125.0	.3546+03	200000	-40.7
19	200	440	318	V. 10.	.3531+03	100 TO 10	4.04-
1048 387 -26.7 -3502.03 -4943.03 -41 108 350 -26.7 -3487.03 -4926.03 -41 1051 349 -27.2 -3458.03 -4912.03 -41 1052 352 -27.7 -3429.03 -481.03 -41 1053 350 -27.7 -3429.03 -481.03 -42 1054 353 -28.2 -3414.03 -481.03 -42 1056 352 -28.7 -3429.03 -42 -42 1056 352 -28.5 -3414.03 -4851.03 -42 1057 352 -28.7 -3371.03 -42 -22 1059 352 -28.7 -3343.03 -47 -42 1059 350 -29.2 -3343.03 -47 -42 -42 1059 350 -29.2 -3343.03 -47 -43 -43 -43 -43 -43 -43 -43 -43 -43 <td>300</td> <td>04</td> <td>34.8</td> <td>7.07</td> <td>. 3517+03</td> <td>FC+0404</td> <td>-41.1</td>	300	04	34.8	7.07	. 3517+03	FC+0404	-41.1
058 350 -26.9 -3472-03 -4912-03 051 349 -27.5 -3463-03 -4912-03 053 352 -27.7 -3463-03 -4861-03 053 352 -27.7 -3463-03 -4861-03 054 352 -27.7 -3463-03 -4861-03 056 353 -28.7 -3414-03 -4851-03 056 352 -28.5 -3460-03 -4851-03 057 352 -28.7 -3366-03 -4851-03 059 352 -28.7 -3346-03 -4851-03 059 350 -29.2 -3343-03 -4772-03 059 350 -29.2 -3343-03 -4757-03 059 350 -29.6 -3314-03 -4757-03 059 347 -29.6 -3314-03 -4757-03 059 347 -29.6 -3314-03 -4757-03 059 347 -30.1 -3258-03 -4757-03 059 340 -30.1 -3258-03 -4757-03 059 340 -30.1 -3258-03 -4757-03 059 340 -30.1 -3258-03 -4757-03 059	00	- 40	30.7	- 24 - 1	.3502+03	1004	-41.3
0 51 349 0 52 346 0 63 352 0 53 350 0 54 350 0 55 350 0 56 351 0 56 352 0 56 352 0 56 352 0 56 352 0 50 352 0 50 352 0 50 354 0 50 357 0 59 357 0 59 357 0 59 357 0 59 357 0 50 343 0 50 357 0 50 343 0 50 350 0 50 350 0 50 350 0 50 350 0 50 350 0 50 350 0 50 350 0 50 350 0 50 350 0 50 350 0 50 350 0 50 350 0 50 350 0 50 360 0 50 360 0 50 360 0 50 360 0 50 360 0 50 360	200		350	-24.0	. 3487+03	4028+01	*-1*-
053 352 -27.7 3443403 -486103 053 352 -27.7 3443403 -486103 056 353 -28.7 -3404403 -486103 056 352 -28.7 -3400403 -485103 057 352 -28.7 -3400403 -483503 057 352 -28.7 -336403 -4861003 059 349 -29.2 -337103 -47203 059 349 -29.2 -3314.03 -47203 059 347 -30.1 -376.03 -474103 058 349 -30.1 -376.03 -4710.03 058 349 -30.6 -3258.03 -4694.03	009	051	340	-27.2	.3472+03	.4912+01	9.1.
053 350 -27.7 -3429+03 +4861+03 056 353 -28.2 -34.9 -03 -4866+03 056 352 -28.7 -3476+03 -4851+03 057 352 -28.7 -346+03 -4820+03 057 352 -28.7 -346+03 -4820+03 059 350 -29.2 -3343+03 -4772+03 059 348 -29.6 -3314+03 -4772+03 058 348 -29.6 -3314+03 -4755+03 058 349 -29.9 -3300+03 -4755+03 058 349 -30.1 -3286+03 -4710+03 058 349 -30.5 -3258+03 -4710+03 059 349 -30.6 -3258+03 -4710+03 059 349 -30.6 -3258+03 -4710+03 059 349 -30.6 -3258+03 -4710+03 059 349 -30.6 -3258+03 -4710+03 050 350 -30.6 -3258+03 -4710+03 050 350 -30.6 -3258+03 -4710+03 050 350 -30.6 -3258+03 -4710+03 050 350 -30.6 -3258+03 -4710+03 050 350 -30.6 -3258+03 -3258+03 050 350 -30.6 -3258+03 050 -30.6 -30.6 -3258+03 050 -30.6 -30.6 -3258+03 050 -30.6 -30.6 -3258+03 050 -30.6 -30.6 -3258+03 050 -30.6 -30.6 -3258+03 050 -30.6 -30.6 -3258+03 050 -30.6 -30.6 -3258+03 050 -30.6 -30.6 -3258+03 050 -30.6 -3258+03 050 -30.6 -30.6 -3258+03 050 -30.6 -30.6 -3258+03 050 -30.6 -30.6 -3258+03 050 -30.6 -30.6 -3258+03 050 -30.6 -30.6 -3258+03 050 -30.6 -30.6 -30.6 -3258+03 050 -30.6 -30.6 -3258+03 050 -30.6 -30.6 -3258+03 050 -30.6 -30.6 -3258+03 050 -30.6 -30.6 -3258+03 050 -30.6 -30.6 -3258+03 050 -30.6 -3258+03 050 -30.6 -3258+03 050 -30.6 -3258+03 050 -30.6 -30.6 -3258+03 050 -30.6 -30.6 -3258+03 050 -30.6 -30.6 -3258+03 050 -30.6 -30.6 -30.6 -3258+03 050 -30.6 -30.6 -30.6 -3258+03 050 -30.6 -30.6 -30.6 -3258+03 050 -30.6 -30.6 -30.6 -30.6 -30.6 -3258+03 050 -30.6 -30.6 -30.6 -30.6 -3258+03 050 -30.6 -30.6 -30.6 -30.6 -3258+03 050 -30.6 -30.6 -30.6 -3258+03 050 -30.6 -30.6 -30.6 -3258+03 050 -30.6 -30.6 -30.6 -3258+03 050 -30.6 -30.6 -30.6 -3258+03 050 -30.6 -30.6 -30.6 -3258+03 050 -30.6 -30.6 -30.6 -3258+03 050 -30.6 -30.6 -30.6 -3258+03 050 -30.6 -30.6 -30.6 -30.6 -3258+03 050 -30.6 -30.6 -30.6 -30.6 -3258+03 050 -30.6	700	0.89		-27.5	*3458+03	.4897+01	# · [# ·
056 353 -28.2 -341403 -4866-03 056 352 -28.2 -341403 -4851+03 057 352 -28.7 -3460-03 -4870-03 057 352 -29.2 -3371+03 -4820+03 059 35 -29.2 -3371+03 -4800+03 059 350 -29.2 -3343+03 -4772+03 059 350 -29.2 -3343+03 -4772+03 059 350 -29.2 -3343+03 -4772+03 059 347 -29.6 -3314+03 -4772+03 059 347 -29.2 -3343+03 -4772+03 059 347 -29.6 -3314+03 -4755+03 059 344 -30.1 -3276+03 -4710+03 058 344 -30.1 -3272+03 -4969+03 059 -30.5 -30.6 -3272+03 -4969+03	000	053	35.2			.4861+03	6.19-
056 352 -28.7 .914.03 .4851.03 058 352 -28.7 .336.03 .4820.03 057 352 -29.2 .3371.03 .4820.03 059 350 -29.2 .3371.03 .4772.03 059 350 -29.2 .3343.03 .4772.03 058 348 -29.4 .3370.03 .4772.03 059 347 -29.9 .3314.03 .475.03 059 347 -30.1 .3276.03 .4710.03 058 344 -30.1 .3276.03 .4710.03 059 344 -30.5 .3276.03 .3276.03	X00.	0.55	000	-28.0	ED+6245	.4866.03	1-21-
-28.5 -3366+03 -4835+03 -4835+03 -4820 -03 -28.7 -28.7 -3371+03 -4820+03 -42 -82 -29.2 -3371+03 -4820+03 -42 -82 -29.2 -3371+03 -42 -42 -42 -29.2 -3371+03 -472+03 -42 -42 -29.2 -3371+03 -42 -42 -42 -29.2 -3371+03 -42 -42 -42 -29.2 -3371+03 -42 -43 -42 -29.2 -3272+03 -42 -43 -43 -43 -43 -43 -43 -43 -43 -43 -43	000	0.56		-28.2	10+#T+c+	.4851.03	-45.3
057 352 -28.7 3371+03 4820+03 -42 059 352 -29.2 33574-03 4724-03 -42 059 350 -29.4 3358+03 472+03 -42 058 348 -29.4 3378+03 472+03 -43 058 347 -29.9 3300+03 4757+03 -43 058 347 -29.9 3300+03 472+03 -43 058 346 -30.1 3272+03 -43 -43.0 -43.0 -43.0 -43.0 -43.0 -43.0	000		266	-28.5	50+00FC •	.4835+03	6.74
10.59	000	057	765	-28.7	50+0555·		•
059 350 -29.2 .3343.403 .472403 -42.05.05.05.05.05.05.05.05.05.05.05.05.05.		0.59	266	-29.0	0.17	**************************************	N (
056 348 -29.6 .3328+03 .472+03 -43 056 357 -29.9 .3304+03 .472+03 -43 059 347 -30.1 .3286+03 .472+03 -43 058 347 -30.1 .3286+03 .4725+03 -43 -30.6 .3258+03 .4720-03 -43		650		-29.2	? ;	.4788+03	6.25
058 357 -29.6 .3314+03 .4741+03 -43 059 347 -29.9 .3300+03 .4741+03 -43 058 346 -30.1 .3286+03 .4725+03 -43 -30.5 .3272+03 .4694+03 -43 -30.6 .3258+03 .4694+03 -43	2005	059		29	7 1	-4772+03	6.21-
059 347 -29.9 -3314-03 -4741+03 -43 -43 -43 -43 -43 -43 -43 -43 -43 -4	00	0.50		~	*3328*D3	.4757+03	-, ,
347 -30-1 +3700+03 +4725+03 -43 -30-1 +326+03 +4726+03 -4710+03 -32 -30-3 +3272+03 +4694+03 -4894+03 -48	8	0.20	05%	-20.0	• 3.314 • 03	.474:40.	-43.1
344 -30-3 -43 -4710+03 -4710+03 -48 -30-3 -3272+03 -4694+03 -4894+03 -4894+03 -48	00	. 450	34.7	1 01 -	• 3300 • 03		-43.8
88*		8 5 0		1.00	.3286+03	1010101	-43-2
.3258+03	1			5005	21	50-01-1	-43.3
				30.6	258	50.4684	

AL TITUDE	WIND SPEED	WIND DIPECTION	JEMPERATURE	PRESSURE	OEMSI 1 v	DEW POINT
. (FT) .	1FT/SEC1	19301	1066 61	(MILL TOARS)	(60AM/H3)	10 9301
330000	0.50	30.0	-30.8	. 3244-03	.4663+03	, <u>~</u>
030100	052	34.2	14101	.3231.03	WD+6844.	-43.4
030200	0.59	340	M 0 000 1	. 3217+03	.4633+03	# * M # 1
030300	190	336	-31.6	3201+03	.4618+63	-43.3
030400	065	336	-31.0	. 3199+03	.4603.03	-
030500	\$0:::	. 335	-32.1	.3176+03	.4589-03	-43.2
03000	190	336	-32.4	.3162+03	.4574.03	-63.1
D YO YOU	890	334	-32.6	.3148+03	.4559+03	0.84-
03000	69 0	# N 1	-32.9	50	******	-42.9
030400	90	33.7	1.11.	. 3123+03	. 4 5 30 + 03	-42.9
031000	***	# MY P	# 0 MM 1	3100+03	* 8515+03	-42.8
031100	. 210		-33.6	. 3095-03	.4500+03	-42.9
031200	110	# MAN	Ø* MM 1	_	.4486.03	0.63.0
Date of the second	110	133	1.46.	•	5D+11+#*	2.54-
20110	2,70			. 3054-03	F0+96m*	N = N = 1
0.000		447	4 1 1 1	. 5041.03	E0+2+44.	
		# W.C.	D 4 PM	. 3028+03	.4427+03	C • 10 ·
- 021100		757	C • SP -	3015-03	. 4412+03	-43.6
		25.5	P*00*	. 5002+03	50+8454·	# · M · ·
0.12000	200		466	50+686Z*	50+585+°	
20000	700	***	D. 50.	50.9162.	5 D+ A96 +	
035186	920	454 · · · · · · · · · · · · · · · · · ·		10+1962	MO+ #5M **	ČI(
003360		707		50.0667	50+0#6#*	
0.42400		225 -	0.001	2037-03	.4326+03	ny.
20,170	100		* * * * * * * * * * * * * * * * * * *	<pre></pre>	50-1164	a.
0.12400	790	11.0	4 684	< 0 - 1 1 4 2 -	50+1476	
012100	100	266	T P P P P	72,44B2.	50+5878	
012400	200	777	9 6 6 7 1	70.850. 70.100.	£2.007F.	
0.129.00	: E	411		20 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2 -	******	
00010		4 2 2	4 42	(O:1007:	50.0777	
033100	100	1 n n		2010103		S
033200	1 02	33.5	0 0 0 P	2823-03	E	
033300	102	335	-39-2	. 2010+03	.4164.03	
033400	5	335	1.01	.2798+03	.4170+03	-45.0
033500	260		-39.7	.27#6.03	.4156+03	-46.1
03 3600	102	336	0.0.	.2773.03	.4143+03	- 46 · 3
	101		2-04-	-2761+03	.*129.03	9.98-
033800	201	6 S 4	5.0.	£0+6#12*	.4115+03	8.94-
033700	EDT.	6	-40.7	.2737-03	.4102·03	-87.1
02100	<u>s</u> :		0 · · ·	\$0.5212.	50+00DF.	-47.3
00000	6 6	5.55 5.55 5.55 5.55 5.55 5.55 5.55 5.5	M = M = 1	.2712.03	.4074+03	5-14-
0074		0 0	0.11	50.007.2.	1900	# * / # ·
2000		237	D ()	2688+D3	*4047+03	0.04-
001110	601		0.5%-	.2676+03	MD+MM D+.	M
005100	777	> C .	-86.5	5 D + W 4 D / ·	*020+03	5.04
034500	71 g	> 0 F		2652.03	.4004-03	7.80-
	111		E - 20 -	2640403	50+56 65	
0.34.00) v	****	M 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	10+8692	.3480403	N. 64
		200		1 0 1 1 0 7 °	. 3488*13	

1001111	1110 37650	TOTAL DIRECTION					
- (1.1)	11/25.61		(0) (0)	(MILLIBARS)	(CANALAS)		(DE 6 C)
03200	116	33.8	-43.6	.2605+03	.3953+03		-49.7
035100	115	139	- # 3 · B	2593+03	.3938+03		-49.8
035200	115	33.7	0.22-	.2582+03	.3924+03		-50.0
075300	118	337.	-64.2	.2570+03	1909+03		-50-1
035400	118	33.9	2.22-	.2558+03	.3895+03		-50.2
035500	110	33.4		.2541+03	.3881+03		-50.3
035600	116	0 MM	V - 88-	3	.3A66+03		-50.5
035700	1.20	11.6	0 4				-80.6
035800	121	336	1 1 1				-50.7
0.14.900	120		P (4)	2561+03	1878+nz		-50.0
034000	121	115		124 GD + C -			;
014100		222	1	10.00.00.00.00.00.00.00.00.00.00.00.00.0	1704603		
034200	1.31	116		FC+F4=F			
01410	777	0.00		50 - 10 T T T	10.00.00		7 1 7
20426	72.	255	7.07.	50.0C.70	50,4045		
	971	P 600		.2446.03	•		9 1 6
036500	126	33.3		ED+88#2*	.3742+03		-52.0
0.3000	1 25	254	6.94-	.2422+03	.3729+03		-52.3
034700	125	333		2411+03	.3716+03		-52.5
036800	126	334	-47.W	.2400+03	.3703+03		-52.7
036900	125	315	-4.7.6	.2389+03	.3689+03		-52.9
037000	125	334	-47.6	.2378+03	.3676+03		-53.1
037100	129	13.5	0.64-	.2367+03	.3661+03	0	-53.1
037200	128	336	E & B -	.2356+03	.3650+03	R	-53.
037300	132	334	-48.5	.2346+03	.3637+03	G	-53.1
037400	1 33	336	6.64-	.2335+03	.3625+03	O	-54.0
037500	130	336	0.64-	. 2324+03	.3612+03	A O	-54.2
037600	1 33	336	-49.2	.2313+03	.3599+03	L R	-54.5
037700	131	33.7	-49.5	.2303+03	.3586+03	F	-54.1
037800	128	33.9	-49.7	.2292+03	.3574+03	·A U	-54.5
037900	132	.336	-50.0	.2282+03	.3561+03	G A	-55.2
039000	1 32	33.7	-50.5	.2271+03	.3548+03	E Ll'	-55.4
038100	133	33.8		.2260+03	. 1515+03	IS T	-55.1
038200	131	33.7	-50.6	.2250+03	.3522+03	3 Y	-55.
D38300	1.32	33.4	-50.6	.2239+03	.3509+03		-56.1
038400	132	33.7	-51.0	.2229+03	.3496+03		-56
034500	1.32	335	-51.2	.2219+03	.3483+03		-56
039600	1 32	335	-51.5	.2208+03	.3470+03		-56
038200	132	334		.2198+03	.3457+03		-56.
036800	131	336	-51.9	.2198+03	. 3444.03		-57.
036900	129	338	-52.1	.2178+03	.3431+03		-57.
029000	1 34	33.2	-52.3	.2167.03	.3419+03		-57.6
039100		334.	-52.5	.2157+03	.3406+03		-57.1
039200	\$4) \$4) \$4)	525	-52.B	.2147+03	.3394+03		-58.1
039300	1.35		-53.0	.2137+03	.3382+03		-58.3
039400	1 36	335	-53.3	.2127•03	.3370+03		-58.6
039500		335	-53.5	.2117+03	.3358+03		-58.8
039600	1 36	135	- 4 3 · B		.3346+03		-59.0
039700	135	33.7	0.45-	097•	.3334+03		-59.1
039800	1 36	135	W • #15-1	.20#7+D4	.3322+03		-59

		. 64.8 -54.8 -55.0	(#ILLIBARS) .2068+03 .2058+03	16PAM/M3) .3299+03 .3287+03	-	(DEG C) -60.0
200 200 200 200 200 200 200 200	13.6 13.7 13.7 13.6 13.6 13.6	-55.0	.2068+03	.3299+03		-60.0
200 200 200 200 200 200 200 200	13.5 13.7 13.7 13.5 13.6 13.6	-55.0	. 20KB+01	.3287+03		. F.O. 2
200 200 200 200 200 200 200 200	33.6 33.7 33.7 33.6 33.6 33.6		CD. 8CD.			1
200 200 200 200 200 200 200 200	33.7 33.7 33.6 33.6 33.6	-55.3	.2048+03	.3275+03		-60.5
500 500 500 500 500 500 500 500	337 333 336 336	- 55 S - 5	.2038+03	.3263+03		-60.7
200 200 200 200 200 200 200 200		B • 66-1	\$0.6202	.3251+03		-609-
200 200 200 200 200 200 200 200	4 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	-26.0	.2019+03	.3239+03		-61.1
000 000 100 100 100 100 100 100	336	2.06.	\$0.600Z.	50+1225.		
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2000 191 2000 191 190 190 190 190 190 190		1.50.	50+0441.	50-5075.		B. 10.
200 200 200 200 200 200 200 200		0.121	1671.03	E0.2616.		-62-1
200 200 139 200 139 200 130 130 130 130 130 130 130 1	336	-57.4	1962+03	.3168+03		-6666-
\$000 \$000	33.7	-51.1	.1952+03	.3156+03		-6666-
\$500 139 500 130 130 130 130 130 130 130 1	338	-57.9	.1943+03	.3145+03		-6666-
130 130 130 130 130 130 130 130 130 130	336	-58.1	1934-03	.3133+03		-6666-
138 139 139 139 139 130 130 130 130 130 130 130 130 130 130	336	-58.3	.1924+03	.3121+03		-6666-
13.0 13.0 13.0 13.0 13.0 13.0 13.0 13.0	337	-58.6	.1915+03	.3109+03		-6666-
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	. 336	E - 05 -	.1906+03	.3098+03		-6666-
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	339	2.65-	.1697-03	.3086+03		-6666-
136 136 136 139 139 139 131 130 130 130 130 130 130 130 130 130	11.9		MO+686"	.3075+03	0 0	-9999-
136 136 136 137 137 137 137 137 137 137 137 137 137			50.6.6.	.00.000.	RI	
136 139 139 139 139 130 130 130 130 130 130 130 130 130 130	36.0	1-66-		10+0401	GI P(- 6666-
136 139 139 139 139 135 135 135 130 130 130 130 130 130 130 130 130 130	3.1	-60.2	1851+03	3020403	N. DC	
139 139 139 139 135 133 130 130 120 120 120 130	339	**09-		.3017+03	Ai DR	-9999.
139 139 139 135 133 130 120 123 123 139 130	781	9.09-	.1833+03	. 3006 + 03	-	-9999.
139 139 131 133 130 120 123 139 130 130 130 130 130 130	340	6.04-	.1824+03	.2998+03	P <i>i</i> QL	-6666-
1 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	34.0	-61.1	.1816+03	.2983+03	\C JA	-6666-
139 131 133 130 130 130 130 130 130 130 130	339	-61.3	.1607+03	.2972+03	ZE LI	-6666-
134 137 135 130 130 126 128 129 116	300	-61.6	.1798.03	.2960+03	T	-6666-
133 133 133 130 126 128 119 116	38.2	-61.6	50+6814	.2949+03	E	-6666-
133 133 130 126 116 111	715	76.50	FD+18/10	20.8662		- 6666-
133 130 130 126 119 119 1113	191	2029-	1763-03	2015-03		• • • • •
3500 133 3500 130 3500 128 3900 123 1000 113	34.1	-42.7	1754+03	.2904.03		-6666-
36.00 37.00 38.00 12.3 39.00 11.9 10.00 11.9	300	-62.9	.1746-03	.2893.03		-0000-
3500 128 3900 123 3900 139 5000 113	339	-63-1	.1737-03	.2462+03		-0666-
3900 3900 11.9 1000 116 1100	339	-63.3	.1729+03	.2870+03		-6666-
3950 119 1100 1113 113	330	-63.6	.1720+03	.2859+03		-000-
ort ort	336	- 6 3 · B	.1712+03	.2848+03		-6666-
	NO (0.44-	.1703-03	.2437+03		-6666-
	338	-64.	10+56-91	-2825+03		-6666-
	200	7-19-	50./801.	-2812+U3		-6666-
1344	118	7 4 4 4	.16/8403	50.0092		-6666
101	111		1462+01	2775.03		. 0000
101	12.0		**************************************	2747401		0000
001	32.7	80.49-	1645+01	2751+04		
102	12 4	6.84-	.1637-03	.2738+03		-6666-
004+400	326	-65.0	.1629+03	.2726.03		-6666-

-65.1	
-65.0	-65.0
6.49	0.201
8-49-	9.49-
- P - P - P - P - P - P - P - P - P - P	
-64.7	1-49-1
9.89	9.79
8.49-	20 - PO-
6.69	6.99-
-65.3	-65.0
65.1-	-65.1-
-65.2	-65.2
4.26-	# 15 P
-65.5	
9.59	6 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4
10 · 10 · 1	8000
1.44-	7.44
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766.	V-661
-67.2	2-19-
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9.19-	9.19-
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200	7 · · · · · · · · · · · · · · · · · · ·
-68.4	# · · · · · · · · · · · · · · · · · · ·
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-66.6	49 * 49 9 ·
-69-	0.69-
0.69-	0.69-
-69.0	0.69-
-69°D	0.69-
-69.0	0.65-
-68.9	68.9
-68.9	6.89
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-68.9	8
-68.0	1 41

Color	11100	WIND SPEED	WIND DIRECTION	TEMPERATURE	PRESSUPE	DENSITY	ō	DEW POINT
		(F1/5EC).	19301	TOE G C I	THILLIBARS)	168AM/#33		10E6 C)
ORIGINAL FACE IS OF POOR QUALITY OF PO	000	9 F (> 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	.1262*03	.2152.03		. 4444
OF POOR QUALITY OF POO		513	2 46		1255*03	66-1417-		
ORIGINAL PRODUCTION OF POOR QUALITY OF POOR QUALITY ORIGINAL PRODUCTION OF POOR QUA	3	210	C FC	C (C (C (C (C (C (C (C (C (C (.144403	50.62120		- 7 7 7 4
ORIGINAL FACE IN OF POOR QUALITY OF POOR QUALITY ORIGINAL FACE IN ORIGIN	000	U67.	970	/ · 100 · ·	1243+03	.2118+03		-6666
ORIGINAL PAGE 131 OF POOR QUALITY ORIGINAL PAGE 131 OF POOR QUALITY ORIGINAL PAGE 131 ORIGINAL PAGE 131	3 6	560	7		1631.03	50.49012		• • • • •
ORIGINAL FACE IS OF POOR QUALITY	٥	930	057	9 • 9 •	-1230+03	2005003		-6666-
ORIGINAL PRODUCE LA CONTROL DE CO	00	920	50 #K	S = 0 = 0	1224-03	*2094+03		-6666-
ORIGINAL FACE IS OF POOR QUALITY				S	-1216+03	.2073+03		6666-
ORIGINAL P	00	051	339	-68.4	.1212+03	.2062+03		-6666-
ORIGINAL P	00		336	# • # 9 -	.1206.03	.2051+03		-6666-
ORIGINAL PAGE 113 OF POOR QUALITY OR POOR QUALITY OF P	00	S#0	336	-68.3	.1199+03	.2040+03		-6666-
ORIGINAL P	00	D#O		-50.5	.1193+03	.2031+03		-6666-
ORIGINAL PAGE 134 OF POOR QUALITY OF POOR QUALITY ORIGINAL PAGE 134 OF POOR QUALITY ORIGINAL PAGE 134 OF POOR QUALITY ORIGINAL PAGE 134 OR	00	0 . 1		-68.6	.1187+03	.2022+03		-9999.
ORIGINAL P	00		326	-68.7	.1181+03	.2013+03		-6666-
ORIGINAL PAGE 134 OF POOR QUALITY OF POOR QUALITY ORIGINAL PAGE 134 OF POOR QUALITY ORIGINAL PAGE 134 OF POOR QUALITY ORIGINAL PAGE 134 OR	00	0.39		-68.8	.1175.03	.2004+03		-6666-
ORIGINAL PROPERTY OF POOR QUALITY OF POOR QUALITY ORIGINAL PROPERTY OF POOR QUALITY ORIGINAL PROPERTY OF POOR QUALITY ORIGINAL PROPERTY OR	00	000	318.	-68.9	.1170.03	.1995+03		-6666-
ORIGINAL P	00	0 0	334	-69.1	.1164.03	.1986+03		-9999-
ORIGINAL PRODUCT CONTROL STATE		039	313	-69-2	.1158.03	.1978+03		-9999-
ORIGINAL PRODUCT CONTROL STATE	00	0.38	313	-69.3	.1152+03	.1969+03		-6666-
ORIGINAL P	00	041	336	-69.5	-1146-03	.1960+03		-6666-
ORIGINAL P.C.: 1000 ORIGINAL	00	0 0	30.5	9.69-	.1140+03	.1952+03	1	-6666-
December 1972 - 1975 -	00		307	-69.8	.1134+03	.1943+03	01 01	-6666-
DOS	8	****	30.2	6-69-	.1129.03	.1935+03	RI F	-6666-
050	00	042	300	-70-1	.1123+03	.1927-03	G! P	-6666-
ALITACOS 1100-03 1100-	00	020	301	-70.3	.1117-03	.1919+03	N 00	-6666-
ALITACOS 1100-003 110		051	30.2	#•0 <u>7</u> -	.1112.03	.1910+03	A) OF	-6666-
100 100	9	980	202	9-04-	1106+03	1902-03	l. ?	-6666-
064 317 -71.0 .1095-03 .1886-03 D64 515 -71.4 .1078-03 .1876-03 D64 515 -71.4 .1078-03 .1876-03 516 -71.4 .1078-03 .1876-03 517 -71.4 .1078-03 .1876-03 518 -71.7 .1075-03 .1876-03 518 -71.7 .1076-03 .1876-03 518 -72.2 .1080-03 .1876-03 518 -72.2 .1080-03 .1786-03 518 -72.3 .1079-03 .1786-03 518 -72.4 .1079-03 .1786	00	057	30.5	-10.8	-1100+03	.1894+03	PQ	-6666-
10 10 10 10 10 10 10 10	00	290	30.7	-71.0	.1095-03	.1996.03	U	-6666-
10	9	#90	33.3	-71-1	.1049+03	-1878+03	C. Al	-6666-
Color	8	9 0	31.5			1870+03	: .I7	-6666-
059 323 -71.5 -1073+03 -1833+03 057 330 -71.6 -1062+03 -186+03 054 331 -71.8 -1054-03 -186+03 052 324 -72.0 -1054-03 -186+03 052 324 -72.1 -1054-03 -1811+03 084 326 -72.3 -1040-03 -1811+03 084 318 -72.3 -1040-03 -1795+03 084 318 -72.4 -1079+03 -1796+03 084 318 -72.4 -1079+03 -1796+03 084 318 -72.4 -1079+03 -1796+03 084 318 -72.3 -1019+03 -1756+03 084 319 -72.3 -1019+03 -1756+03 086 319 -71.8 -9931+02 -1755+03 085 313 -71.4 -9931+02 -1756+03 086 316 -71.3 -966+03 -1756+03 086 316 -71.3 -966+03 -1756+03 086 316 -71.3 -966+03 -1756+03 086 316 -71.3 -966+03 -77.3 086 -71.3<	Da		125	# 1 <u>7 -</u>	.1078+03	•1862+03	[3 [Y	-6666-
057 330 -71.7 -105/-05 -1186-0	8 8	290	32.3	50 m h l	1073+03	1853+63	1	-6666-
054 330 -71.6 -1056-03 -10750-03 052 324 -72.0 -1065-03 -1019-03 047 326 -72.2 -1045-03 -1011-03 047 318 -72.3 -1040-03 -1040-03 046 318 -72.4 -1035-03 -1795-03 046 316 -72.4 -1024-03 -1766-03 047 318 -72.4 -1024-03 -1766-03 048 319 -72.3 -1024-03 -1766-03 047 309 -72.3 -1014-03 -1766-03 050 319 -72.0 -1014-03 -1766-03 1766-03 -72.0 -1014-03 -1766-03 1766-03 -72.0 -1014-03 -1766-03 1766-03 -72.0 -1014-03 -1766-03 1766-03 -72.0 -1014-03 -1766-03 1766-03 -71.7 -1014-03 -1755-03 1775-03 -71.7 -998-003 -1755-03 1775-03 -71.4 -998-003 -1755-03 1775-03 -71.4 -998-003 -1755-03 1775-03 -71.4 -998-003 -1759-03 1775-03	9 6	. 050	7.5	9.1/1	50.7.601.	EG - CHET -		-6666-
052 334 -72.0 -1045-03 -1016-03 047 326 -72.1 -1040-03 -1011-03 047 326 -72.3 -1040-03 -1011-03 046 318 -72.3 -1050-03 -1795-03 046 316 -72.3 -1024-03 -1796-03 -72.4 -1079-03 -1776-03 -1776-03 040 314 -72.3 -1074-03 -1766-03 -72.4 -1019-03 -1766-03 -1766-03 -72.4 -1019-03 -1766-03 -1766-03 -72.4 -1019-03 -1766-03 -1766-03 -72.4 -1019-03 -1766-03 -1766-03 -72.4 -1019-03 -1756-03 -1756-03 -72.4 -1019-03 -1756-03 -1756-03 -72.4 -1019-03 -1756-03 -1756-03 -72.4 -1019-03 -1756-03 -1756-03 -72.4 -1019-03 -1756-03 -1756-03 -72.4 -1019-03 -1756-03 -1756-03 -72.4 -1019-	3 6	750	23.0	1-11-	50.7401.	50+95×1.		-9999
047 326 -72.1 .10405.03 .1811.03 047 325 -72.3 .10400.03 .1795.03 046 316 -72.4 .1029.03 .1796.03 046 319 -72.3 .1024.03 .1766.03 -72.4 .1024.03 .1756.03 .1766.03 -72.4 .1014.03 .1756.03 -72.4 .1014.03 .1756.03 -72.4 .1014.03 .1756.03 -72.4 .1014.03 .1756.03 -72.4 .1014.03 .1756.03 -71.4 .1003.03 .1756.03 -71.4 .998.00 .1756.03 -71.4 .998.00 .1756.03 -71.5 .988.00 .1756.03 -71.4 .998.00 .1756.03 -71.5 .998.00 .1756.03 -71.5 .998.00 .1756.03 -71.5 .71.1 .998.00	3 6	0.54	155	0.77	20.00.01.	10.0101		-0000-
047 325 -72.7 .1040+03 .1795+03 046 316 -72.4 .1035+03 .1795+03 046 314 -72.3 .1024+03 .1786+03 -72.4 .1024+03 .1776+03 .1776+03 040 319 -72.1 .1019+03 .1766+03 040 310 -72.0 .1014+03 .1756+03 050 317 -71.4 .1003+03 .1755+03 051 312 -71.4 .998-0.07 .1755+03 051 316 -71.3 .988-0.07 .1755+03 051 316 -71.3 .988-0.07 .1755+03 051 316 -71.1 .988-0.07 .1755+03	: 8	640	12.6	-73.1	1045401	1011+03		-0000-
047 318 -72.3 .1035.03 .1795.03 046 316 -72.4 .1024.03 .1766.03 046 319 -72.1 .1024.03 .1766.03 047 308 -72.0 .1019.03 .1766.03 048 310 -72.0 .1019.03 .1766.03 050 317 -71.4 .1003.03 .1755.03 051 312 -71.4 .998.2.02 .1755.03 053 312 -71.4 .998.0.02 .1755.03 051 316 -71.3 .9880.00 .1755.03 051 316 -71.1 .9880.00 .1755.03	90	100	32.5	-72.2	.1040+03	.1903+03		-6666-
046 316 -72.4 .1029.03 .1766.03 044 314 -72.3 .1024.07 .1776.03 046 309 -72.1 .1019.03 .1756.03 -72.1 .1019.03 .1756.03 .1756.03 050 319 -71.7 .1019.03 .1755.03 050 313 -71.4 .9982.02 .1755.03 051 312 -71.4 .9982.02 .1755.03 053 312 -71.4 .9981.02 .1715.03 051 316 -71.3 .9860.02 .1705.03 -71.1 .9879.02 .1765.03	00	047	318	-72.3	.1035-03	.1795+03		-6666-
044 314 -72.3 .1024+07 .176+03 046 309 -72.1 .1019+03 .1766+03 046 310 -72.0 .1014+03 .1755+03 050 309 -71.7 .1003+03 .1755+03 050 312 -71.4 .9982+02 .1755+03 051 312 -71.4 .9981+02 .1755+03 051 316 -71.3 .9860+02 .1705+03 -71.1 .9879+02 .1705+03	00	9#0	316	-72.4	.1029+03	.1786+03		-6666-
046 309 -72.1 .1019.03 .1766.03 047 308 -72.0 .1014.03 .1755.03 1046 319 -71.4 .1003.03 .1755.03 1050 339 -71.7 .1003.03 .1755.03 1051 312 -71.6 .998.2.02 .1755.03 1051 316 -71.3 .988.0.02 .1755.03 1048 318 -71.1 .987.9.02 .1755.03	2	0 44	31.4	-72.3	.1024+03	.1776+03		-6666-
047 308 -72.0 .1014.03 .1755.03 046 310 -71.8 .1003.03 .1745.03 050 339 -71.4 .1003.03 .1755.03 050 312 -71.6 .998.2.02 .1755.03 051 316 -71.4 .9931.02 .1755.03 051 316 -71.3 .9880.02 .1755.03 -71.1 .9879.02 .1755.03	00	9#0	300	-72.1	.1019+03	.1766+03		-6666-
046 317 -71.8 .100A+07 .1745+03 050 329 -71.7 .1003+03 .1755+03 050 312 -71.4 .9931+02 .1755+03 051 316 -71.3 .98P0+02 .1705+03 -71.3 .98P0+02 .1705+03 -71.3 .98P0+02 .1705+03	00	7+0	30.8	-72.0	.1014-03	.1755+03		-6666-
050 329 -71.7 .1003+03 .1735+03 .1735+03 .1735+03 .1735+03 .1725+02 .1725+03 .1725+0	00	9.0	31.0	-71.A	.1008-03	.1745+C3		-6666-
050 113 -71.6 .9982.02 .1725.03 .1725.03 .1725.03 .1715.0	2	0.50	33.9	-71.7	.1003+03	.1735+03		-6666-
053 312 -71.4 .9931-02 .1715-03 .051 316 -71.3 .98F0-07 .1755-03 048 318 -71.1 .9629-02 1695-03	9	0.50		-71.6	20+2#66*	2		-6666-
051 316 -71.3 .98P0.02 .1705.03 048 318 -71.1 .9879.02 1695.03	2	053	31.2	-71.4	.9931+02	.1715.03		-6666-
D 048 1695+F39879+D2 1695+F3	00	051	316	-71.3	.98PO+02	.1705-03		-6666-
			318	-71.1	.9829.02	8		-6666-

					DEWSITY	DEN POINT
		STEED STREETTON	TEMPERATURE		CERAN/R31	13 9301
AL TITUDE	WIND SPEED	Ì	(DEG C)	CHILLIAMS!	1485+03	-++++
	1F1/5EC1.	1	-71.0	20.61.6	1478+03	-0466-
255000	0 4 2		-71.2	20+6216	104174	-6566-
044100	0.19		-71.0	20.6196.	F C 4 3 4 5	-6666-
066200	037	323	-71.6	.9629+02	200000	-6666-
	0.35	523	-71-8	.0580+02	FC - 1501 -	-6666-
2000	0.32	330	-72-0	.9531+02	50+1591	. 6666-
	0.32		-13.2	.9482+02	*******	-6666-
-	0.28	32.6	-72-4	.9433+02	501/541	-6666-
022900	0.26	12.6	-72-6	. 9385+02	1630+03	.600
00000	024	33.4		.9337.02	10.5.01	6666-
	024	111	0.17	. 9289+02	1617-03	-6666-
023700	026	33.7	4000	.8822+02	.1534.03	6660-
	0.31	12 A		.8377+02	10+B981	-0000-
non rea	025	331		.7954+02	104441	*****
	010	721	5 42	7551+02	1324 +03	
Toron S	010	31.2	9.00	.7170-02	1245+03	- 66661
00000	0.22	111		.6814+02	.1162+113	
061000	021	32.1		-6480+02	.1093+03	
062000	210	320	7.00-	4164+02	.1035+03	
000 90	416	30.8	1.69-	5865+02	.9835+02	
000490		29.1		5580+02	.9384+02	
000990	210	295	2.00	5309+02	.0915-02	
000990	410	30.	7.00-	. 5052+02	.0411+02	****
000200	410	318	1	-4809+02	7001	
	910	32.7	1000	.4579+02	7544+02	. •
200000	016	33.2	-62.6	.4359+02	20.2121	-6666-
071000	110		-61.6	.4151+02	16.00 B4.	-6666-
012000	011	7 50	-60.2	3954-02	20-00-0-	-6666-
07 1000	011	7.50	0.65-	.3767-02	5865+02	-0000-
014000	010		6.65-	20+0404	.5576+02	******
075000	600	02.2	-59.	30-13-6	.5283+02	-6666-
016000	460	510		20.0876.	.5019+02	*****
017000	and a	110	-57.5	1042407	.4763+02	- 6666
01000	68	-10	-56.5	2825.07	.4524+02	-666-
.019000	500	02.1	155.0	20+5692	.4296-02	- 6666
000000		030	9	2571+02	.4087-02	
000180	000	23	0.86.	2453+02	.3892+02	
082000	800	8 CO	9.00	2340+02	. 3696+02	
DESCO	010	6 81:	9.761	2234+07	3502.02	
000+80			6.00.	.2113+02	. 3330+02	
08200	810	303	3.00	.2037-02	.3173-02	
	910	288		.1945+07	.3017+02	
00000	20	27.7	4-7-4-	.1858+02	70+0197	-6666-
	025	268	. ^	.1775+07	20.08.12.	•6660
000000	0.30	5 9 3	S 4 2 4 1	.1696+02	2011002	-6666-
00000	0.33	192		.1630+07	20-1957	-6666-
00550	0.35	797	-42-0		201052	-6666-
000100	037	457	-39.7	1520+02	2167+02	-6666-
000+60	0.30	967	-37.5	.1455+07	:	
000500	0.82	1				

DEW POINT					-	•														• • • •			••••	C)F		PO)(R	(QL	JA	L	Ţ	Y	-0000	-000					•			000			-000			
0645174	.2052+02	.1960-02	.1973-02	1788.02	.1701-02	.1416.02	.1536.02	.1463-02	.1401-02	.1351+02	1300-02	.1257.02	.1206-02	.1149.02	.1092-02	.1037-02	. +665+01	10.41.4.	. 9031-01	.8662+01	10-8620	.7433-01	1203-01	.7251+01	.6935+01	.6640-01	.4371.01	.6117.01	. 5674-01	. 5641+03	11-91-95	.5194-01	10.000	10.00	10.01.01	. 4265-01	. 4102-01	.3945-01	.3794-01	.3649+01	3504+01	1314-01	. 3745+01	.3120-03	2995-01	.2868+01	10.4472.	.2625-01	.2516.01		
PRESSURE	1491-02	1111002	.271.00	1223+02		•	1076-02	1012+02	10-000	00000	10+001+	6722401	10.4214	10.0104	74.010	7165-01	7067-01	6702-03	4510+01	6249.01	. 5999-01					4903+01	4711.01	. 6577+03	4350.01	. 6181.01	. 4018-01	.3861+01	.3711+01	. 3547.01	3629-01	3248401		10+4000	2012-01	2703+01	.2597-01	.2446.01	.2398-01	10.5010	.2215+01	.2129+01	2046+01	.1967-01	.1001.01		
TEMPERATURE	וטנפ כז	5.96-		0.00-		1.55-	0-16-	1.62-		1-12-	-28.3	0.01	R-1151	7.016.1	-20-	-58-1	-52-	-23.0	5-22-	0.22-	2-12-		7.07-	•	- 1 I	•••1-	V-61-	6.61-	7.61-		0.611		70 7 T	9 m - 1	•	-14.2	•	4.61-	F	_:	? :	_ :	2 1	2 :	~ 4	0.01-	9 4	1.01.			
MIND DIRECTION	Ä	32	251	35	25.7	7.82	25.0	33.	754	22.7	202	239	23.0	24.1	20.7	**	280	265	- 270	77.3	214	27.0	. 102	202	282	200	278	212	266	76.1	25.7	255	287	52	7	ž.	×	25.	25.9	26.0	592	111	216	612.	2007	280	719	27.4	717	276	
		200		930								100		1.20		100						961		2	6	****	200	200		1	200	760	0.50	*0	80	\$						52.5	2	5	9	4			155	551	
	111106	(FT)	00000	000160	00000	000660	100000	101000	102000	103000	104000	10500	104000	10200	10000	10400	11100	11, 000	112000	113000	114000	115000	114000	117000	116000	119000	1 20000	121000	122000	123000	000421	125000		00000	124000	1 30000	131000	132000	133000	134000	1 36,000	1 36000	1 3 7000	1 18000	90067	1 * 6000	1 1000	0002 • 1			· AAREAT.

	•																								C)R)F	IG F) (1)	IAI OI	L R	P. Q'	AC U/	JE AL	 T	Ş Y												
DFW POINT	_	-6666-	-6666-	-0000-	-1111	-9999	-4666-	-9999.	- 1000		- 6666-	-6666-	-0000-	-1999.	-000-	-0666-	-1000-	-0460-			-	-9999.	-9999.	-1111	-6666-	- 666			-6666-	-9999.	-666	-1111	-000-	-4444		-9999.	-1999,	-6666-	-4664-	-1999.	-1111	-000-	• 6660:	-666-	-0466-	-0000	-1999.
DFRSITY	(MX/X40)	.2420+01	.2330+01	.2239+01	.2139+01	.2045+01	. 1956+01	10-11-01	10+2091		.1605+01	.1544+01	1485-01	.1929+01	.1375+01	1323+01	.1273+01	.1225.01	10+6/11+	100201	10,101,	1011101	.9735+00	.9370+00	. 9033+00	1105-00	00.4858.	00,404	.7502+00	.7208+00	.6925+₽0	.6653+00	.6394+00		56.78.00	.5460+00	-5249+00	.5072+30	1 1 - 00	.4754+00	9	00+00	.4316+00	.4175+00	. 036 • 00	5 :	00.2575.
PRESSURE	(MILLIBARS)	.1819+01	1749+01	.1682+01	.1616.01	ż	.1497-01	10+10+11	10+1851.	10.0001.	.1237+01	.1191+01	.1146+01		.1062+01	.1022+01	.9842-00	.9475+00	00.2214.			.7838+00	.7547+00		. 6997+00	00+1679	00+400	00+1104	-5787+00	.5571+00	.5364.00	.5165+00	00+4264	00+04/4		. 4280+00	.4123+00	.3972+00	.3826+00	. 3684+00	.3547+00	00+2+2N	.3286+00	13161+07	. 3041+00	00+5262	. 2513+00
TEMPERATURE	(0.00)	-11.3	-11:0	-11.4		0.4-		7-5-			. L. W.	5.4	8.8-		-4-1	3 · # ·		P. M. 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		7 P P P P P P P P P P P P P P P P P P P	g pri	- 3 - 1	-3.1	-3.0				7 4 () ()		-3.9	-3.3	-2.1	-2.1	- 1 - 2			ın•	K*-	-1.9	-3.5	-5.0	# () - ()	9-1-	er /	-10.1		-
WIND DIRECTION	ā	27.5	27.3	270	26 7	266	265	* 92	26.0	7 9 7	264	26.3	26.1	240	25.9		25 d	25.R	25.3	26.1	26.2	26.4	26.6	26.4	264	26.3	797	26.1	26.1	26 1	260	26 3	26.4	202	26.1	25.7		25.3	25 5	26.0	262	26.3	262	22.0	052	1 BY	542
WIND SPEED	•	160	162	163		991	77	2 Z Z	100		1.60	140	182	188	187	1.90	5	1 20	202	217	233	234	212	5 04	216	827	254	246	246	286	5*6	249	942	2.39	251	268		261	288	243	299	952	2 2	AB 7	253	197	
AL T I TUDE	(FT)	146000	147000	0000	000001	000001	151000	152000	154000	000331	154000	157000	1 \$4000	159000	160000	161000	162000	163000	000491	166000	3.6.7000	16000	169000	170000	000171	000771	2000	175000	176000	177000	176000	179000	180000	181000	1 8 3000	184000	185000	186000	187000	168000	169000	000041	191000	000241	000561		TANKE TO THE TANKE

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PRESSURE	(HILLIBARS)	.2190-01	-2070-01	1960-01	.1860-01	.1770-01	.1680-01	1590-01	-1510-01	10-02-1	-1360-01	1290-01	.1220-01	-1160-01	1100-01	1050-01	•1000-01	.9500-02	20-0004.	-8600-02	-8200-02	. 7800-02	7400-02	- 1000-02	. 6 700-02	20-0019	70-00 - 5-		-5300-02	.5000-02	-4800-02	-4500-02	* 303-02	4115-02	20-5646	\D-00.00	· 3440-02	.3290-02	.3146-02	. 3008-02	.2877-02	.2751-02	. 2630-02	-2515-02	-2405-62	-23:00-02	376	249	.1447-02
	LOEG C)	-H	7078	2.26-	7.58	262-	~	-42-2	2.28	-61.2	S - O - O	2.08-	5.87-1	C-1/-	1007	7.8/1	****	2.17		8.60	4 44	-66.2	-65.2	-64.2	-64.2	63.2	-61.6	-61.1	9.65-	2.96-	- 40.7	4.04-	-61.9	-63.1	-64.4	-65.7	0-19-	-68.3	9-69-	8 · D/ ·	1.27	-74.7	0.94-	-77-2	-78.5	-79-1	-78.5	-77-	
WIND DIRECTION	25.9	25.6	222	287.	282	23.5	727	217	306	195	185	717	169	162	157	153.	••	187	14.5	143	205	142			7 4	166	107	150	154	160	160	16.8		• • •		17.1	17.	- 176	179	- 162	187	194	R	0.27	25	246		512	
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•	10-4961	.2392-04	0.4.0	132	5+0	400000
- 6666	-2187-04	.2570-04	102.2	129	160	397000
	.2437-04	.2768-04	9.00	125	**0	394000
-6666-	.2724-04	*5-6862*	79.2	121		391000
- 6666-	* 3054-04	.3237-04	68. 0	11.9	045	366000
	#0-98#M.	. 3517-04	57.1	115	0.46	3.85000
*****	. 3977-04	.3832-04	46.6	112	9+0	382000
- 6666-	*0-685 *·	. 4188-04	36.4	109	840	379000
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	.5763-04	.5165-04	19.1	114	052	373000
-6666-	*0-629 9 *	.5760-04	10.9	104	050	370000
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-6666-	1009-03	*0-8*6L		980	063	1,5,10,00
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-0666-	.1380-03	.1037-03	-24.4		20	355000
-0000-	.1615-03	.1194-03	-29.8	101	0.33	352000
-666-	.1890-03	.1351-03	-35.2	D34	90	
-1000-	.2211-03	.1542-03	-40.6	1 600	027	146000
-0666-	.2596-03	.1771-03	-45.0	130	001	1000
-0000-	.3058-03	.2051-03	-48.3	26.2	0.25	140000
-6666-	.3602-03	.2374-03	-51.7	26.6	D47	337000
-0000-	.4244-03	.2747-03	-55.0	26.8	062	14000
-6666-	.4999-03	.3178-03	-58.3	26.9	071	000111
-6666-	.5889-03	.3577-03	-61.7	26.9	110	12-000
-1111	.6931-03	.4271-03	-63.8	269	116	125000
-6666-	.0159-03	.4960-03	-65.9	269	1 38	122000
-0666-	.9603-03	.5760-03	-68.0	269	152	000611
•666-	.1130-02	.6688-03	-70.1	269	1.58	000411
-6666-	.1330-02	.1765-03	-72.2	269	9	20011
-6666-	.1567-02	.9052-03	-73.8	27.0	141	110000
-0666-	.1847-02	.1059-02	-75.0	27.1		
-6666-	.2177-02	.1238-02	-74.2	27.2		20000
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DEN POINT	DFNSITY	PRESSUPE	TEMPEPATURE	MIND DIRECTION	MIND SPEED	A1 7 17 UDG

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(67)	181/18	CAFE	1000			
070000	120	222			1000000	
00100	200	636	6067	10.1701.	70.0011.	7 • 0 1
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	141	339	-46.2	.2275+03	. 3492+03	707
	133	338	9.84-	.2173+03	. 3371-03	-62.2
	132	330	-50.2	.2075+03	. 3242+03	-63.3
	107	340	-52.1	.1980+03	. 3121+03	-64.7
	153	340	154.5	1889+03	. 3010+03	-
	9.1	339	-56.6	1.001+03	10.000	460.2
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;		4		204727		7.01
		***	/ ·C-	• 1030 • US	50+9697·	* · D. / -
	103	332	-58.3	.1559+03	. 2528+03	-70.1
	105	332	-58.6	. 1 4 4 4 0 3	. 2412+03	01-
	104	333	-59.2	10.9141.	2 10K+M1	-

ALTITUDE	MIND SPEED	MIND DIRECTION	TEMPERATURE	34053344	DE#5177	DEN POINT
(14)	(FT/SEC)	(056)	IDES CI	(WILLIBARS)	(6PAN / N 3)	() 9301
050000	106	133	-51.1	.1284 • 03	.2110-03	-0000-
051000	101	332	-62.2	.1223.03	. 2020 • 03	- 4000
052000	140	332	-62.7	1165		
083000	600	MMM	-63.4	1109.0		-9466-
054600	076	13.00	~	1055	1709-03	
055000	910	***	-52.6	1005+0		-9999.
054000	270	334	-63.0	.9567.02	. 1586+03	-0000-
051000	073	335	-63.3	•	.1512+03	-9999.
000000	073	335	-64.2	0	. 1445-03	-9999
024600	075	335	2.49.	.8251.02	. 1377-03	-9999
000090	0.10	336		.7852.02	.1310+03	-1000
06160	0.10	335	-64.1	.1473-02	. 1245.03	-1000-
042000	270	335	-63.1	.7114.02	.1180+03	-0000-
063000	07.	335	-62.2	2	.1119-03	-6666-
000190	110	334	-61.2	•	. 1040+03	-9999
000590	090	335	-6.65-	.6144-02	. 1004-03	-6666-
000990	000	336	-50.7	.5855.02	. 9511-02	-4444
067000	075	336	-57.6	.5580+02	. 9018+02	-4444
06.000.0	990	333	-56.5	.5320.02	. 8554 + 02	-9999.
D00490	050	328	-55.6	.5073+02	.8124.02	-9999
070030	054	327	-24.0	.4838+02	. 1722 - 02	-1199
071060	600	328	-53.8	.4615-02	. 1329 - 02	-000
072060	640	330	-53.0	. 4 403 - 02	.6967-02	-1111
073000	053	333	-52.1	. 4 202 • 02	. 6622 - 02	-1000
07.500	150	333	-51.0	. 0111.02	.6290+02	-9999
075000	047	331	-50.1	.3029.02	. 5980-02	-9499
076000	140	329	****	.3656.02	ċ	-4444.
077000	**0	329	9.84-	.3492+02	.5418+02	-0666-
074000	052	331	-47.9	.3335+02	. 5154 • 62	-0000-
079000	053	333	-47.2	.3196.02	. **12*02	-0666-
000000	050	333	0.94-	. 3044-02	. 4668 - 02	- 6666
081000	140	330	-15.1	.2909+02		-1000
005500	8 0	332	-44.2	.2781+02	. 4232+07	- 6666-
063000	020	M (5.00 m	.2659+02	20.00	- 6666-
00000	. • 0	332	1 0 1 0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	20.2052.	3843.02	
020500	\$ 4 0	329		20+1592	20+2995	-
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000490		n • •	*****		20+ PC05 .	
00000	170	210	**************************************		70-6007	
041000	240	308	10 mm	10.00-05	2717-02	-0666-
900240	040	DOX	38.		29.878.02	-6666-
00240	0.70	295	-11.0	.1648+02	20+0+02	
000140	0 36	290	-37.6		. 2292+02	- 40 64
000540	2+0	582	-37.0	20-02-11	. 2169.02	- + + + + -
000460	••0	200	- 16.5	.1393+02	Ö	- 6666-
00140	0.55	275	0.92-	.1334+02		-0000-
00000	050	210	9.82.	77	-	-2000
000440	190	265	- 24.6	.1223.02	.176, +02	

(FT) (FT/SEC) (F	260 260 259 259 247 242 242 241 241 241 250 260 260 260 273 282 282 282 282 282 282 282 282 282 28	066 C) 1 3 3 1 1 2 4 1 1 2 4 1 1 2 4 1 1 1 2 4 1 1 1 1	. 1172 + 02 . 1172 + 02 . 1175 + 02 . 1032 + 02 . 9 9 9 9 + 01 . 9 100 + 01 . 9 100 + 01 . 9 100 + 01 . 7 6 5 + 01 . 7 6 5 + 01 . 7 6 5 + 01 . 5 7 6 0 + 01 . 5 7 7 0 + 01 . 7 7 0 + 01	. 1701 + 02 . 1701 + 02 . 15 16 + 02 . 16 16 + 02 . 17 16 + 02 . 18 16 + 02 . 19 16 + 02 . 10 16 + 02 . 10		
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	259 259 247 241 259 259 250 273 273 275 282 282 282 282 282 282 282 282 282 28		.1123+02 .1076+02 .9898+02 .98082+02 .9100401 .8122+01 .7880+01 .7885+01 .7885+01 .7885+01 .5799+01 .5799+01 .5799+01 .5799+01 .5799+01	1516+02 1536+02 1161-02 1130+02 1130+02 1130+02 1127-02 110		
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	254 247 242 239 239 241 241 241 241 242 242 242 242 242 242	- 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2	.1032.02 .9492.01 .9402.01 .9100.01 .8702.01 .766.01 .765.01 .6510.01 .5799.01 .5799.01 .5799.01 .5799.01	1463+02 1304+02 1304+02 1374+02 1206+02 1206+02 1092+02 109		
	247 242 239 239 241 241 242 242 242 242 242 242 242 243 244 244	224 - 1	. 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	. 1961 + 62 . 1351 + 62 . 1257 + 62 . 1256 + 62 . 1266 + 62 . 1092 + 62 . 109		
	242 238 241 241 241 259 273 273 282 282 282 282 282 282 282 282 282 28	1 1 2 2 2 2 3 3 3 3 3 3 3 3 3 3 3 3 3 3	. 9 4 9 2 + 01 . 9 1 0 0 + 01 . 8 1 7 2 4 0 1 . 8 0 1 0 0 0 1 . 7 0 6 7 + 0 1 . 6 5 1 0 + 0 1 . 5 7 6 0 + 0 1 . 5 7 6 0 + 0 1 . 5 8 3 1 + 0 1 . 5 8 3 1 + 0 1 . 6 2 1 4 0 1 . 7 1 0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1351+02 11504+02 11204+02 11204+02 1164+02 1164+02 1164+02 1164+02 1164+02 1164+02 1164+02 1164+02 1164+02 1164+02 1164+03		
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	238 241 247 259 265 273 273 274 282 282 282 282 282 278 278 278 278 278	1 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	. # 722 + 01 . # 8 152 + 01 . # 6 100 + 01 . # 7 6 5 + 01 . # 5 10 + 01 . \$ 7 9 9 + 01 . \$ 7 9 9 + 01 . \$ 5 10 + 01 . \$ 10 1 + 01 . \$ 7 10 + 01 . \$ 7 10 + 01	12:7402 11206+02 1194+02 1194+02 1093+01 9919+01 9919+01 9919+01 1952+01 1753+01 1753+01 1753+01 1753+01 1753+01 1753+01 1753+01 1753+01		
	241 254 259 265 265 273 273 282 282 282 282 282 282 282 282 282 28		. 6 55 6 0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	. 1206 + 02 . 1164 + 02 . 1092 + 02 . 1031 + 02 . 1031 + 02 . 96 19 + 01 . 94 19 + 01 . 94 19 + 01 . 95 25 + 01 . 75 3 + 01 . 75 3 + 01 . 75 1 + 01 . 64 40 + 01 . 64 40 + 01		
	247 259 260 240 270 273 279 281 282 282 282 282 282 282 282 282 286 278 278 278 278	- 30.4 - 28.1 - 25.6 - 22.3 - 22.3 - 20.2 - 14.9 - 15.9 - 15.9	. 460000 . 766000 . 766000 . 676000 . 651000 . 651000 . 57600 . 57600 . 510300 . 510300	. 1195-02 . 1092-02 . 1092-02 . 9965-01 . 9913-01 . 9913-01 . 7913-01 . 7913-01 . 7581-01 . 7581-01 . 6915-01		
	259 260 245 270 275 279 282 282 282 282 282 282 282 282 282 28	28.5 20.2 20.2 20.3 20.2 20.3 20.2 20.3 20.3	.7680+01 .7565+01 .7067+01 .6780+01 .65190+01 .5760+01 .5760+01 .5760+01 .5760+01	. 1092 + 62 . 1033 + 62 . 9449 + 61 . 9449 + 61 . 9449 + 61 . 754 + 61 . 754 + 61 . 754 + 61 . 69 35 + 61 . 69 35 + 61 . 69 35 + 61 . 69 35 + 61		
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	265 273 273 274 275 282 282 282 278 278 278 278 278 278 278	22.0 22.0 22.0 22.0 22.0 22.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1	. 7067+01 . 6782+01 . 6249+01 . 5949+01 . 5949+01 . 5312+01 . 5312+01 . 5401+01	9965+01 9919+01 9625-01 7953+01 77593+01 77593+01 77593+01 77593+01 77593+01 77593+01 77593+01 77593+01 77593+01		
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	273 276 279 281 282 282 280 272 272 266 266	-222-2 -221-3 -120-2 -120-2 -150-9 -150-9	. 5 2 4 9 + 0 1 . 5 2 4 9 + 0 1 . 5 7 6 0 + 0 1 . 5 3 1 2 + 0 1 . 5 1 0 3 + 0 1 . 4 7 1 1 1 + 0 1	. 9031401 . 8662 01 . 793401 . 7583 01 . 7581 01 . 6935 01		
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	262 262 262 260 272 272 266 266	100.2 100.2 110.6 110.6 110.6 110.6 110.6	.5551-01 .5512-01 .5103-01 .4903-01	. 75 U + 01 . 75 U + 01 . 75 U + 01 . 6		
	282 282 280 278 272 266 266	4 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	.5511+01 .5312+01 .5103+01 .4903+01 .4711+01	.7563+01 .7251+01 .6935+01 .6-40+01		
	282 280 280 272 266 266	**************************************	.5103+01 .5103+01 .4903+01 .4711+01	. 7251 • 69 US • 60 US • 60 US • 61		
	280 278 272 266 266		.5103+01 .4903+01 .4711+01	• 6935-01 • 6<40+01 • 6 - 11+01		
	272 272 266 266		.4903+01			
	272 272 266 2641	S S S S S S S S S S S S S S S S S S S	.4711+01	.6.1101		
	266	-15.3	10-111-01			
,	265	-15.3	127401			
	702		401111111	10+111-)F	
		1.61	10+065+	10+1/05	•	
	162	-15.0	. 4 181 +01	. 5641+01	P(
	\$62	-14.1	.4018.01	. 5416+01	D(
	152	-14.2	.3861+01	10+0610	AI CF . SEE-	
	652	-13.7	.3711+01	. 4984+01	· ~	
	260	-13.8	.3567+01	.4792+01	P Q	
	259	-14.0	.3429+01	10+609+	AU.	_
131000 111	259	-14.2	.3296.01	. 0434+01	GIA	_
132000	258	4.41-	. 3168+01	. 4265+01	L	_
33000 116	258	-14.6	. 3044+01	. 4102+01	""	ľ
34000 123	258	-14.7	2926+01	. 3945+01	, Y	•
35000	260	-15.0	.2812+01	1794+01		
	265	-15-1	2703+01	10+6498	0000-	
137000	271	P (S)	.2597+01	15.00+01	••••	
	276	3.51.0	2404401	1000000		
	270		104401			
1 =				10.64.75		
		D 0 0 7 1	10+60620	10.0215.	*****	
•		n.	1016177	10+6447	• • • • • • • • • • • • • • • • • • • •	
		07 11	10.4212	10-2927	- 4444-	
	278	-13.4	.2046-01	.2744+01	-6666-	
155	277	-12.1	.1967.01	.2625+01	-1000-	
150	276	-11.3	.1891+01	.2516+01		
106000	275	M 4 17 1	1819+01	.2420+01	-0000-	
	273	9-11-	1749+01	2330+31		
198000	270		5	2239431		
	247					

DEN POINT	-			. 6666-	*****	- 6666-	- 6666-	-6666-	-6666-	-6666-	- 6666-	-6666-	-0000-	-6666-	-6666-	-6666-	6660	- 6660-	0000	6000	0000			• • • • • • • • • • • • • • • • • • • •	0000			9000		0000	0000	5000				0000		0000			0000		-6666-		0000	6666-		0000	0989		*****	- 4444-		
DENSITY	GRAM/M3)	. 2045+01	. 1956+01	. 1877+01	. 1602+01	. 1734+01	1668+01	1004071		1885+07	1829+01	1175+01	10454		10.5121	10.6771	10.6/11.	. 1134+01	1002+01	. 1051+03	1011-01	. 9735+00	.9370+00	. 9033+00	.8705+00	.8389+00	. 8086+00	.1792+00	.7502+00	.7208+00	.6925+00	.6653+00	. 6394+00	. 6143+00	20+6065	. 5678+00	. 5460+00	. 5249+00	. 5072+00	. 4913+00	. 4759+00	00+109#	00+25+4	00+015	00+6/14	- 403e	3894+00	. 3752+00	. 3610+00	. 3476+00	. 3345+00	. 3219+00		
PRESSURE	(MILLIBARS)	1556+01	1497+01	10+1441		10.1001.	10+6551.	10+5821.	.1237+01	10+1611	10+911.	11103+01	1062+01	10-2201	.9842+00	.9475+00	.9122+00	.0783+00	.0456+00	.0141+00	7838+00	7547+00	7267+00	A007+00	4737+00	00+9847	00+m29	6011+00	4787+00	5571+00	5 364 +00	5165+00	00+4764	4790+00	4613+00	00+***	.4280+00	.4123+00	3972+00	.3826+00	. 3684+00	.3547+00	.3414+00	.3286+00	.3161+00	.3041+00	.2925+00	.2813+00	2705+00	2602+00	2502+00			
				6.91	-5.7	1-5-	6.4-	9.4.	7.4-	5.4-	***	-4.2	-4.1	0.41	6-8-	7-8-	7-11	- # · · · · · · · · · · · · · · · · · ·	7 4 100	r M	7 • • •	100-	1.5.	•	m*m-	6.6-	0 · M		* * * * * * * * * * * * * * * * * * *	* G		7.5.	1.2-	1.2-	0.71	7-1-	0.1	•		1 0	3 P		4	0 1	1	101-		0.11.	0.21-	-12-1		-12.6	9.71-	
	MIND DIRECTION	(930)	266	265	264	264	26.	476	107	107	507	107	0 0 0	637	967	258	258	260	263	. 261	292	269	266	264	264	26.3	262	261	261	261	261	260	263	264	265	265	261	257	254	253	255	260	292	263	292	952	250		245	247	252	254	255	
	LING SPEED		841		7.1	175	177	180	160	180	160	182	101	187	190	194	199	202	207	217	233	23.0	217	900	707	920	210	986	206		286	200	0 40	246	210	201	251	268	271	261	248	243	244	246	249	249	253	261	260	202	229	216	214	
		ALITIMOE		150000	151000	152000	153000	154000	155000	156000	157000	158000	159000	160000	141000	142000	000,7	00000	000491	000691	000991	167000	168000	169000	170000	171000	172000	173000	174000	175000	176000	177600	178000	179000	180000	161000	000201	00000	184000	185000	00000	0000		00000	000001	000141	DOUZAL .	00000	00000	000561	196000	197000	000001	199000

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	(FT/SEC)	(0E6)	(066 C)	(MILLIBARS)	(SRAH / H3)	1056 C)
200000	219	255	13.0	2313+00	3067+00	
201000	226	256	-13.7	.2224+00	2004490	
202000	226	256	- 17.0	2110000	201410	
203000	214	255	0.41-	2056+00	2444	-
204000	199	255	9 4 1	0047401	00-11-1	
205000	185	25.8	-12.		00+1697	
204000	175	25.0			00.0145	
201000	175	255	K 177	00.8781	00+96+7	- 6466-
20400	1 4 4	0 10 10	115.3	1,58+00	.2357+00	• 6666-
20000		167	A - 1 -	00+0401	. 2240+00	-6666-
21000		607	1.01-	1624+00	. 2206+00	-6665-
21100	Y84	707	-10-	1561+00	. 2130+00	-000-
	181	112	-50.0	1444+00	- 2010+00	-6466-
THE PERSON	787	273		.1440+00	. 1998 • 00	-0000-
213000	186	272	-23.0	.1363+00	. 1926+00	-0000-
714000	195	272	-24.3	.1327+00	. 1858 - 00	-0000-
215000	204	27.1	-25.5	.1274.00	. 1792+00	-0666-
216000	212	271	-26.4	.1223+00	.1727+00	-0000-
217000	221	272	-27.8	1173+00	1665+00	
218000	229	279	-29.2	1125+00	1401+00	
219000	234	276	-31.2	00101		
22000	238	278	1 1 1 1	1020400		
221000	236	270	-15.2		000000	
222000	239	279	1.41		00.461.	
223000	220	7.1.6	6.66		00.4367	
224000	226	276	2000		00-1621	
225000	224	27.1	2.6.4.	10-00-1	00-1111	IC.
226000	224	24.1	7.11	10-0077	70+0111.	•
227000	229		1000	10-0000	00-1401-	
224000	276		70.00	10-000¢	10-6/96	•
22000	270		200	10-00/6	. 9332-01	•
2 10000	146	111	7 • 6 6	10-0016	10-9669	•
231000	200	27.0	7.99	10-0016	10-1968	•
232000	206	310	2.69-	10-000	10-1029	U
21100	200	216	7	10-0564	10-32-01	•
218000	2 40	0 4	2.57	MD-D05 # *	10-96+7	•
245000	2.40	216		10-040+·	1182-01	•
24000	241	0 1	7.0/1	0-0600	10-7000	•
217000	222	213		10-044C-	10-1969	
238000	212	0.7	6.07	10-0066	10-4529	• • • • • • • • • • • • • • • • • • • •
216000			7.6/-	10-025	10-2046	
240000	9 6	2 2 2	7.61	10-0015 ·	10-6/96 ·	-000
20100		2.4		EO-042*	10-8956+	*****
2000	701	0.7	2.03-	.2840-01	. 5126-01	-0000-
200040	n) T	692	0.18-	.2700-01	10-1484	-0000-
247000	B 1	197	-81.2	. 2560-01	10-5+94	-1111
200447		592	-81.2	.2430-01	10-6044	-0000-
245000	135	262	-81.2	.2300-01	. 4173-01	-9999.
246000	123	259	-81.2	.2180-01	. 3955-01	-6666-
247000	113	256	-82.2	.2070-01	. 3776-01	-9999.
24000	193	252	-82.2	· i éé à .		
			,	١	10-3/65	

TABLE 5. (Continued)

																						•	0	R	IG P	O.	AA Ol	L R	ł Q	'بر ال	G Al	E LI	is																
DEV POINT													- 6666-	- 6666-	-0000-	- 6666-	-9999	-4444-	-0000-	-1111	-9999-	-4444	-100	-9999-	-9999.	-1000	-1000	• • • • • • • • • • • • • • • • • • • •	-0000-	-6666	- 4444	-6666-				****	-1000-	-1666-	-1000-	-0000-	-1000	-4664-	-6666-	-9999.		-9666-	7998	-9099	-0000-
OE BSITY	10 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	10-6436	10-2/06	10-0047	10-10-7	10-6467	10-0212	10-10-6	10-6950	10-4007	10 42 41	10-3545	10-029	. 1546-01	10-4781	. 1306-01		. 1245-01	_	.1117-01	. 1067-01	. 1012-01	.9552-02	. 9036-02	. 1645-02	. 0139-02	. 7014-02	. 7331-02	. 7010-02	-6703-02	.6410-02	20-6219	20-10 FC •	30-00ec	4124-62	20-1064	.4686-02	. ***1-02	. 4285-02	- 4098 - 02	. 3918-02	. 3747-02	- 3746-02	. 3025-02	.2566-02	.2117-02	. 1847-02	. 1567-02	. 1320-02
PPESSURE	1910101	10-0//1:	-,					10-0771	10-0771	•	10-0301	10-0001	10-0011	\$000-02	.9600-02	.8200-02	.7000-02	.7400-02	.7000-02	.6700-02		.6100-02	.5800-02	. 5500-02	. 5 300 - 02	20-0005	20-0094	20-005**	. 4373-02	20-5118-05	. 1935-02	.3763-02	20-8465 ·	30-0-0-	20:0476	3000-02	.2877-02	.2751-02	.2630-02	.2515-02	.2405-02	. 2 300 -02	.1970-02	.1692-02	.1447-02	.1230-02	.1059-02	. 9052-03	.7765-03
TEMPEDATUPE	1025	7.50-	9.70	7.4.6		V C C C C	n ()	7.0	6-11-	4 4 4	6.46.	4 64	-71-2	-70-3	4.49-	-67.5	9.99-	-56.5	-65,2	-64.2	-54.2	-63.2	-61.6	-61.1	-59.6	-59.5	-59.2	-59.3	-40.6	-61.9	-63.1	# · # · · · ·	7.00	200		- 70	-72.1	-73.4	-70.7	-76.0	-77.2	-78.5	-79.1	-78.5	-77.4	-76.2	-75.0	-73.8	-72.2
MINC DIRECTION	7 4 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	262		127	717	5 4 3 0 4 7		74.1	• • • • • • • • • • • • • • • • • • •	75.2	15.7		661	1.1	145	100	142	142	191	343	19.2	143	199	147	150	154	160	75	160	697	690	170	1/1	44	44.0	179	182	107	100	204	220	242	206	244	275	272	271	270	269
MIND SPEED	(71/520)			6 (6)				040		7 4		***	180	****	700	100	092	240	092	0.01	680	***	082	710	27.0	065	000	055	150	9 0	140		037		170	920	020	017	•10	011	\$ 00	\$00	010	028	074	117	150	3.5	160
ALTITUDE	20000	25.000	000167	200257		26600	264.000	25,7000	25.000	254000	20007	261000	262000	263000	264000	265000	266000	267000	26.8000	26+000	270000	271000	272000	273000	279960	275000	276000	277000	276000	279000	280000	000182	000292		2000	284000	287000	288000	289000	29000	291000	292000	245000	0 90962	301000	30+060	30 7000	310000	313000

TABLE 6. STS-5 SRB DESCENT-IMPACT SURFACE SHIP OBSERVATIONS

	Wind Speed Kt.	22	ORIGINAL OF POOR	FAGE I S QUALITY		Ht. m. 2%
	Wind Direction	020。	Visibility (miles)	٢	Swell Conditions	Dir. from which Swell Freq. is coming Sec. 7
	Pressure (MSL) mb	1022.6 (60° station press = 1020.8 mb)	Total Opaque Sky	5/10		Ht. Dir m. whi
	Dew Point °F	9	Total Sky Cover	5/10	Wind Waves	Freq. Sec. 7 C (75.2°F)
USN Ship, Gen. H. S. Vandenberg n: 29°N Latitude 78°W Longitude November!1,1982 1226 UT Observation:	Wet-Bulb °F	68.0	Clouds	1s at 1,800 ft	[]	Sea Moderate – Code 4 4/10 Breaking Waves 2/10 Foam Surface Sea Water Temp. = 24.0°C (75.2°F)
Site: USN Ship, Gen. H. S. Location: 29°N Latitude 78°W Longitude Date: November !1, 1982 Time: 1226 UT Surface Observation:	Air Temp. ° F	75.0	Sky Observation:	5/10 Cumulus at 1,800 Sea Observation:	Sea Condition	Sea Moderate — Code 4 4/10 Breaking Waves 2/10 Foam Surface Sea Water Tem
N J G F N			<u>v</u>	Š		

TABLE 7. SELECTED ATMOSPHERIC OBSERVATIONS FOR THE FLIGHT TESTS OF THE SPACE SHUTTLE VEHICLES

	Count Down and	Launch Comments of Meteorological Significance			Wind directional change observed at Pad just prior to L+0.8		
Inflignt Conditions Max. Wind Below 60,000 ft		Dir. (deg)	250	286	250	329	336
		Speed (ft/sec)	86	158	119	37	146
		Alt. (ft)	44,300	36,300	45,000	47,900	40,600
Surface Observations Thermodynamic ^a Wind ^b	d _l	Dir. (deg)	125 120	345 355	50f 145f	133 ⁱ 141 ⁱ	8 8
	Wind	Speed (ft/sec)	11.8	27.0	7.0 ^f 8.0 ^f	5.8 ⁱ 4.9 ⁱ	22.0 35.0
	e _o	Rel. Hum. (%)	82	61	1.1	70	89
	Temp.	21	23	24	29	22	
	Тћет	Press ^d N/cm ²	10.234 ^e	10.166	10.160	10.200	10.227
Vehicle Data		Launch Pad	39A	39 A	39 A	39A	39A
	Time ^c (EST) Nearest Mınute	0020	1010	1100	1100 ^h	6110	
	Launch Date	4/12/81	11/12/81	3/22/82	6/27/82	11/11/82	
	Vehicle No.	STS-1	STS-2	STS-3	STS4	STS-5	
		S. S.	-	2	т	4	\$

a. Pad 39A thermodynamic measurements taken at approximately 1.2 m (4 ft) above natural grade at camera site No. 3. b. 1 min average prior to L+0 of 60 ft PLP (listed first) and 275 ft FSS winds measured above natural grade.

c. Eastern Standard Time unless otherwise noted.

d. Pressure measurement applicable to 21 ft above MSL unless otherwise indicated.

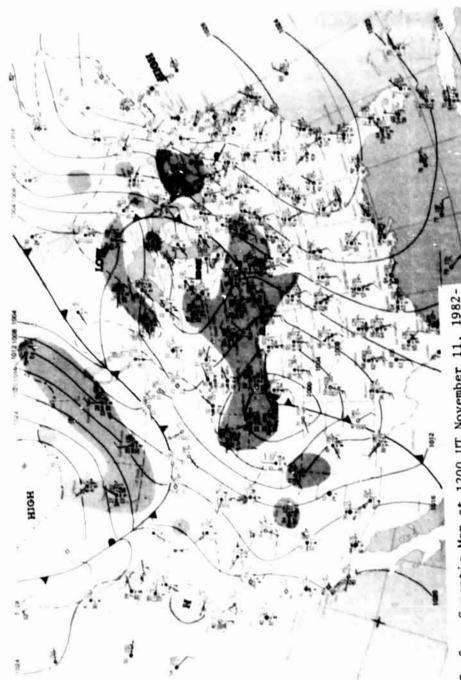
e. Pressure measurement applicable to 14 ft above MSL.

f. 10 sec average prior to L+0.

g. Due to onset of sea breeze. h. Eastern Daylight Time.

i. 30 sec average prior to L+0.

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Surface Synoptic Map at 1200 UT November 11, 1982-Isobaric, Frontal, and Precipitation Patterns are Shown in Standard Symbolic Form.

Figure 1. Surface synoptic chart 19 min prior to launch of STS-5.

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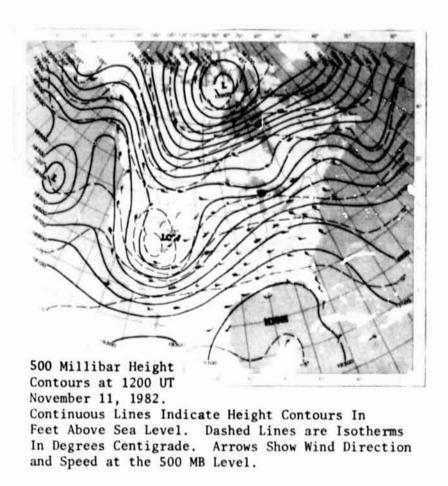


Figure 2. 500 mb map 19 min prior to launch of STS-5.

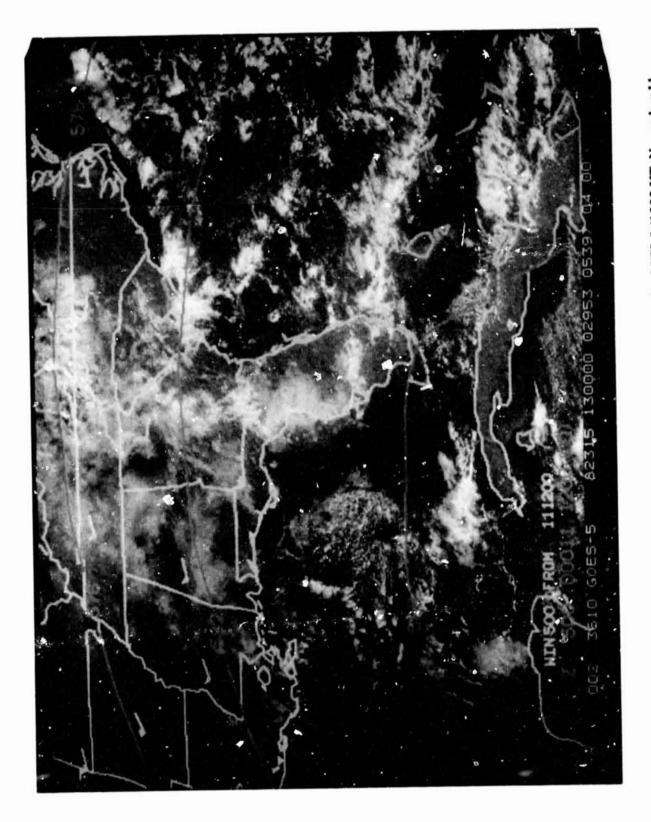


Figure 3. Goes-5 visible imagery of cloud cover 41 min after launch of STS-5 (1300 UT, November 11, 1982). 500-mb contours and wind barbs are also included for 1200 UT.

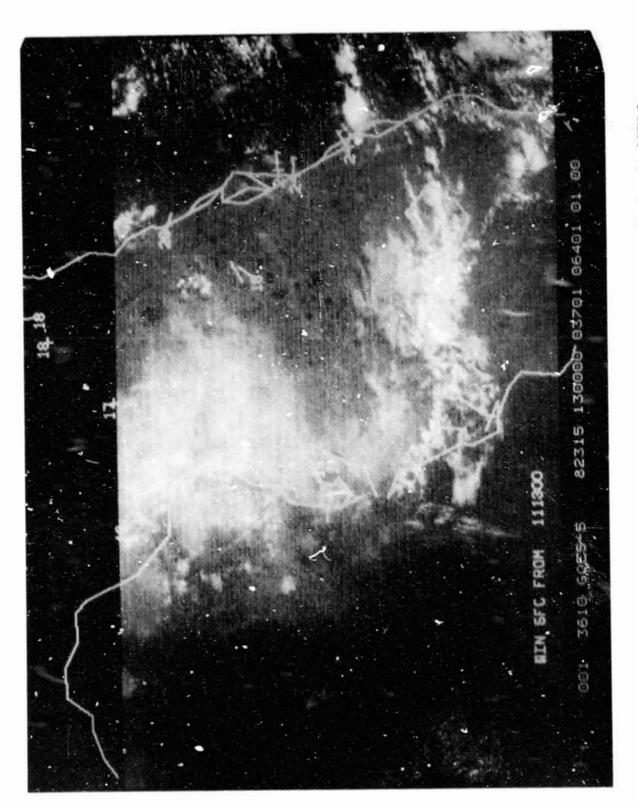


Figure 4. Enlarged view of GOES-5 visible imagery of cloud cover 41 nán after laur * of STS-5 (1300 UT, November 11, 1982). Surface temperatures and wind barbs for 1300 UT are a... included.

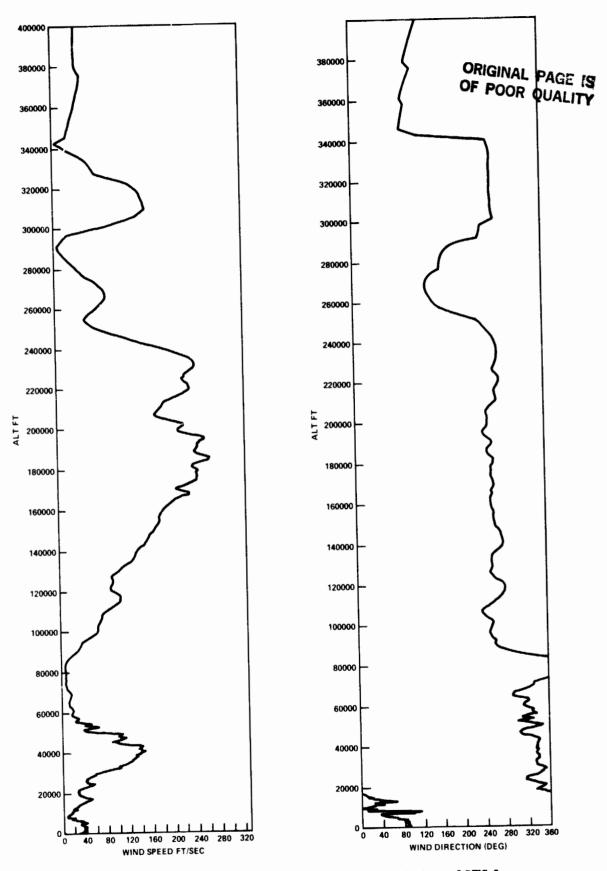


Figure 5. Scalar wind speed and direction at launch time of STS-5.

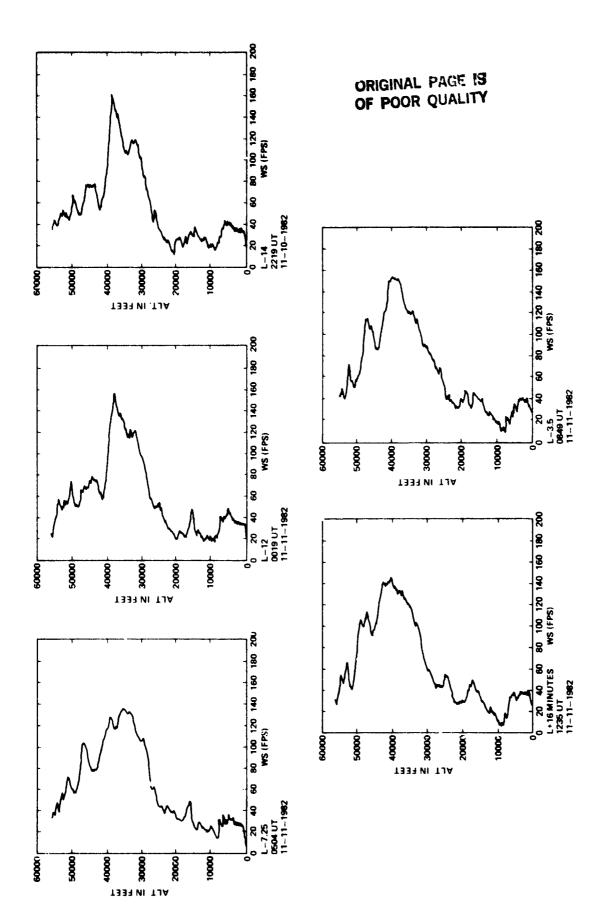
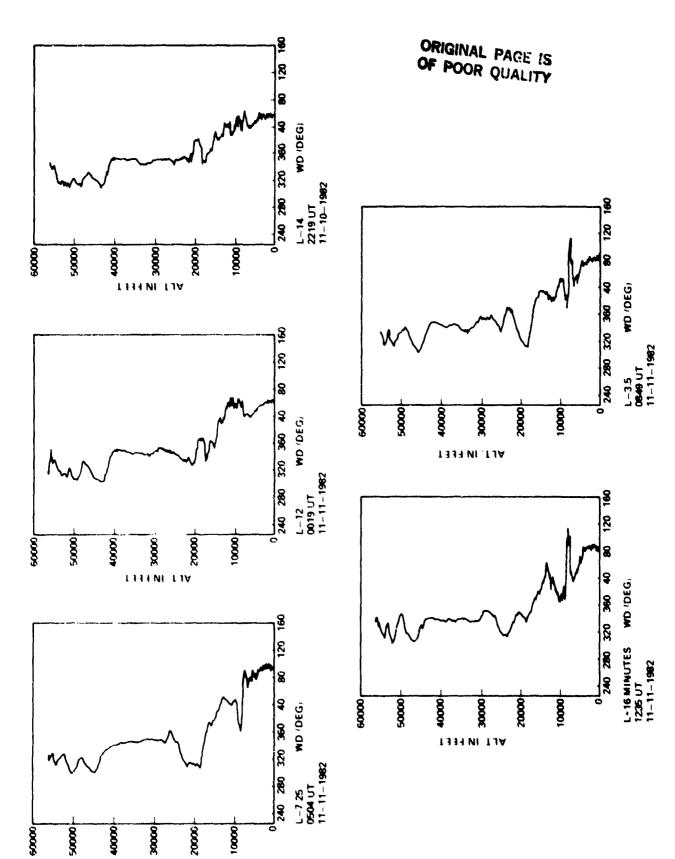


Figure 6. STS-5 prelaunch/launch Junsphere-measured wind speeds (FPS).



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Figure 7. STS-5 prelaunch launch limsphere-measured wind directions (degrees).

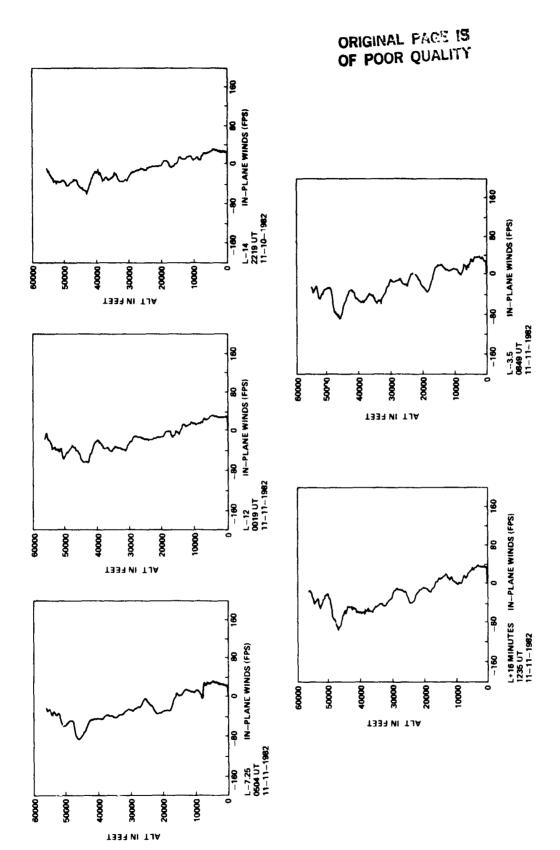


Figure 8. STS-5 prelaunch/launch Jimsphere-measured in-plane component winds (FPS). Flight azimuth = 90 degrees.

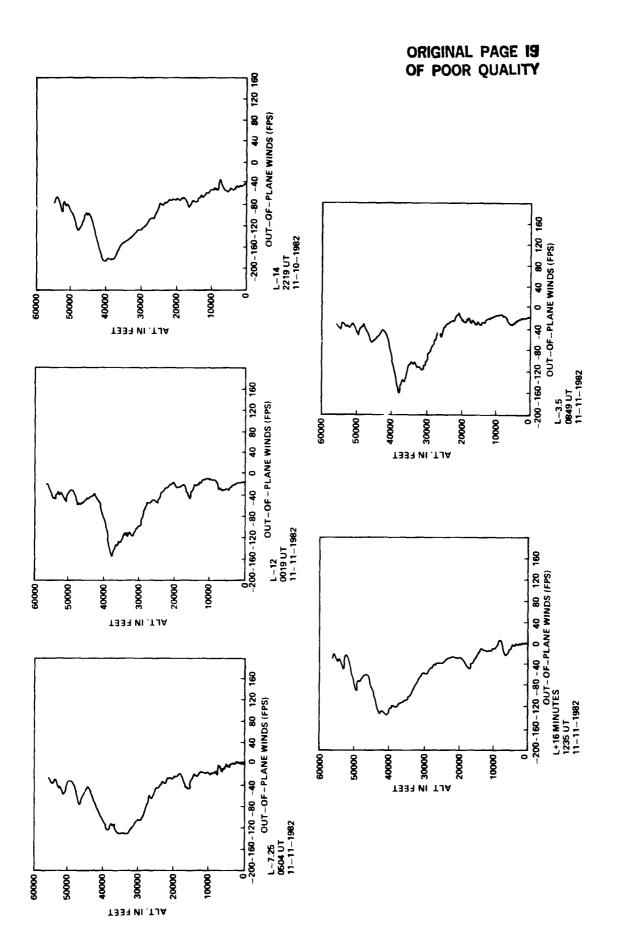


Figure 9. STS-5 prelaunch/launch Jimsphere-measured out-of-plane component winds (FPS). Flight azimuth = 90 degrees.

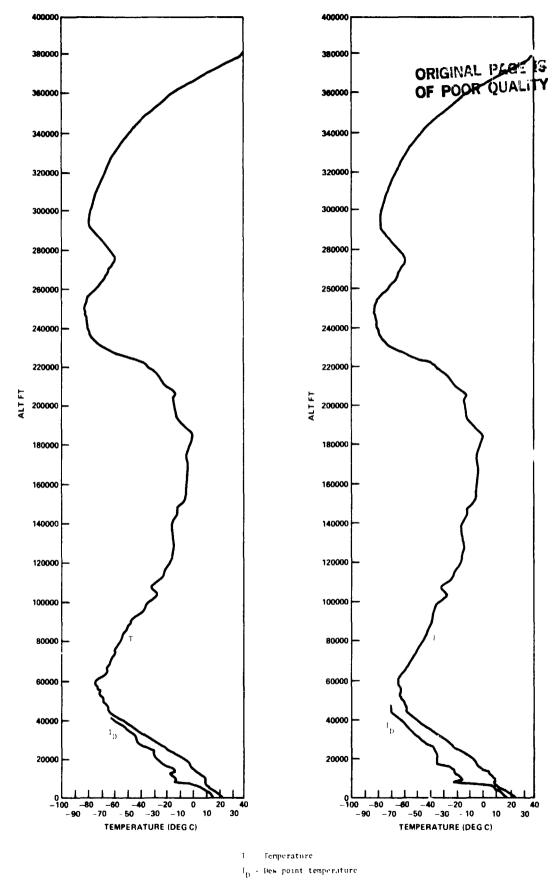


Figure 10. STS-5 temperature profiles versus altitude for launch (left) and SRB descent (right).

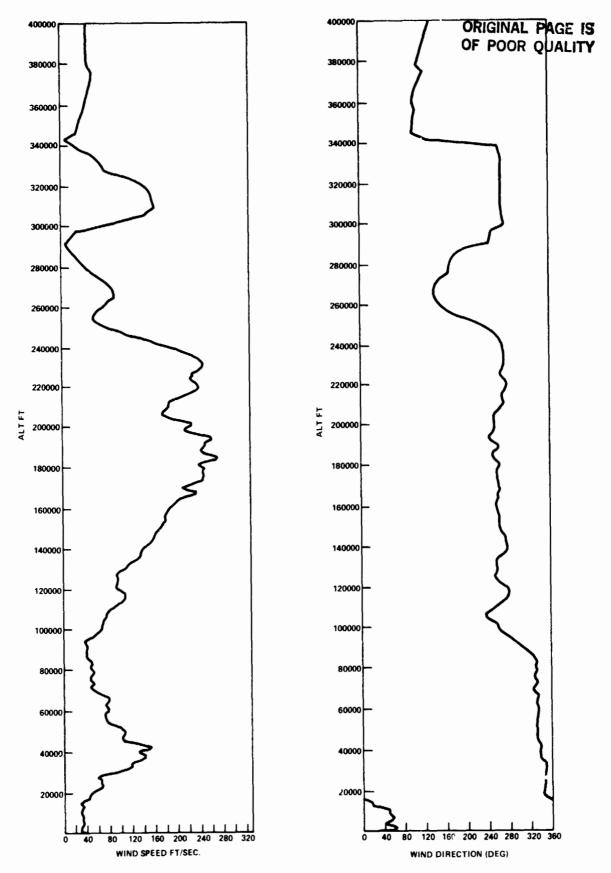


Figure 11. STS-5 scalar wind speed and direction for SRB descent.

APPENDIX A

UPPER ATMOSPHERIC CHANGES INFLUENCING STS-5

SUMMARY

Relatively strong wind profiles were observed in the 20,000 to 40,000 ft altitude STS-5 high dynamic pressure layer above KSC from L-14 through L+0 hr. As an illustration at L-14 hr a maximum windspeed profile value of 160 ft/sec associated with a direction of approximately 350 deg produced left crosswind values of approximately 160 ft/sec at approximately 39,000 ft altitude. This translates into a probability of less than 1 percent that this crosswind speed would occur based on historical data records. Some vehicle load indicators indicated values exceeding the earlier designated 100 percent capability as a result of this wind. The large increase in crosswind component between the L-26 and L-14 hr Jimsphere as shown in Figure A-1 was not anticipated from information available at the time of the L-24 hr LSEAT [(Shuttle) Launch Systems Evaluation Advisory Team] meeting. However, from examining the routine 1200 UT (6 a.m. CST) 10 November upper atmosphere analyses by NOAA, it is apparent that stronger NNW winds were likely over Central Florida at launch time than was evident from information available at the L-24 hr LSEAT meeting. When these analyses became available, 11 a.m. CST (L-19 hr), and if a procedure had been established, an updated advisory of the anticipated wind speed change could have been made to the LSEAT. In the future, if desired, it may be possible to reduce such surprises to the LSEAT in the period prior to L-14 hr if routine meteorological analyses are made available in a more timely manner using one of the interactive display systems such as McIDAS. This concern diminishes in importance beginning about L-14 hr because it is then that Jimsphere measurements become more frequent and the statistical risk for changes in the inflight winds for L+0 are incorporated as an allowance in the knockdown load dispersion calculations.

KSC AREA ATMOSPHERIC PATTERNS INFLUENCING STS-5 ACTIVITIES

The following is a synopsis of the atmospheric conditions which existed during the STS-5 count-down, some comments relative to the Prelaunch Wind Loads Monitoring Team's advisory role on expected inflight wind changes, and recommendations to improve inputs for LSEAT decisions.

The synoptic or large scale upper-atmosphere atmospheric pattern affecting the U.S. during STS-5 countdown (L-50 to L+0 hr) was dominated by an intense center of low pressure over California. A jet stream or band of strong winds (speeds approximately 185 ft/sec at 40,000 ft) associated with this system was oriented about this cyclonic center. This wide belt of high winds was indicated off the California coast arching southward and then eastward across the California Baja, then northeastward into New Mexico. Another upper atmosphere trough of low pressure was situated off the Atlantic coast of the U.S. east of the Florida peninsula. A ridge or area of higher pressure between these two cyclonic systems was present over Florida and surrounding region. The above-described synoptic pattern can be seen on a series of 200 millibar constant pressure analyses (approximately 40,000 ft altitude) presented here for 1200 UT 9 November, 1200 UT 10 November, and 0000 and 1200 UT 11 November 1982 (Figures A-2 through A-5).

THE INFLIGHT WIND SPEED CHANGE PREDICTION DILEMMA

It is characteristic of an atmospheric condition such as described above that, once established, a high degree of persistence may exist for several days. The wind direction during the STS-5 countdown sequences (L-50 to L+0) was, in fact, relatively persistent. However, significant wind speed increases, and especially left crosswinds, were measured by Jimsphere and rawinsonde balloon systems between L-26 and L-14 hr. The wind speeds associated with the deep layer of northerly wind directions produced large crosswind components above KSC and load exceedences in excess of the earlier designated 100 percent capability on some indicators. To anticipate this particular change in the atmospheric condition successfully for periods of 24 to 48 hr, the energetics of the large-scale, complex, low pressure system located near the California coast must be correctly assessed.

The wind speeds produced at 40,000 ft and other altitudes by this pressure system were directly related to a complex thermodynamic pattern existing within this large system. Perturbations of wind, temperature, humidity, and density propagated downwind (eastward, in this case) affected conditions at considerable distances from the cyclonic center. The development and timing of events on a mesosynoptic scale are difficult to anticipate even with the large-core computers and sophisticated models used by NOAA. This particular problem was compounded due to changes in the thermodynamic and wind field structure over the eastern Pacific where quantitative data are extremely sparse. Seemingly minor perturbations emanating from the large-scale trough altered dramatically the wind speed profile characteristics over the U.S. including KSC.

A point to keep in mind is that the rawinsonde profile data on the synoptic scale are measured routinely by NOAA only at 0000 UT (6 p.m., CST) and 1200 UT (6 a.m., CST). In addition, the 1200 UT data analyses, for example, do not become available through normal NOAA transmission channels for use until about 1700 UT (11 a.m., CST) or a lag of 5 hr. A post-flight analysis of the 1200 UT data (L-24 hr) for 10 November indicated that increased crosswind speeds could have been anticipated and the information provided to the LSEAT by L-19 hr if the most current analyses had been available earlier.

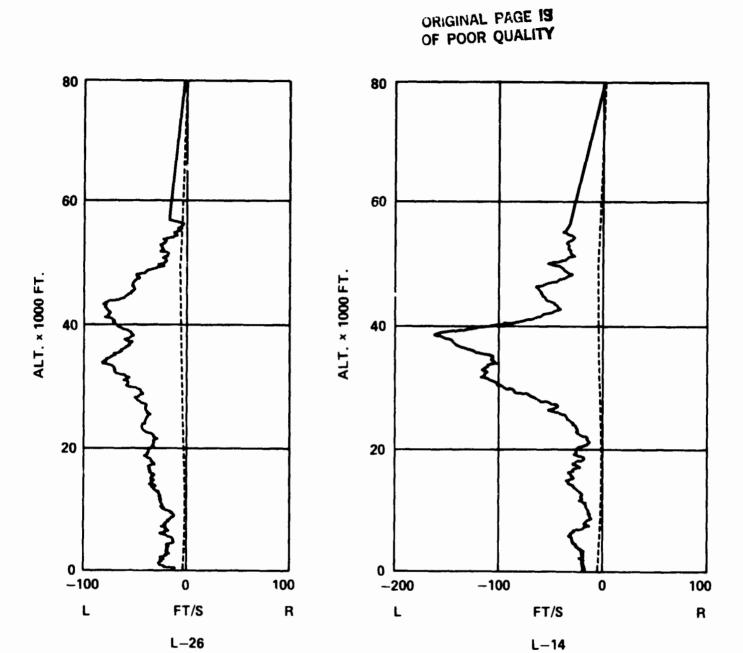


Figure A-1. STS-5 out-of-plane wind component time history.

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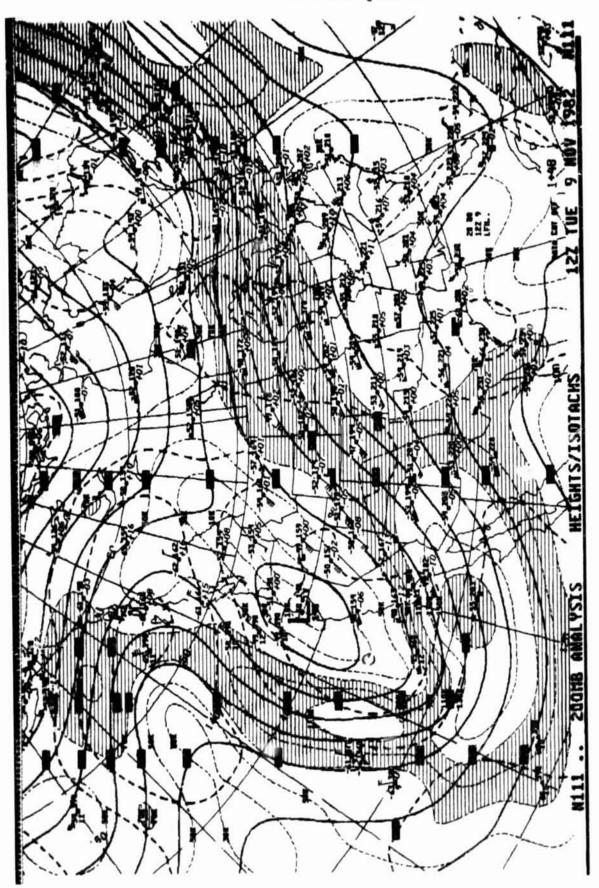


Figure A-2. 200 mb upper-air analysis for 1200 UT, 9 November 1982.

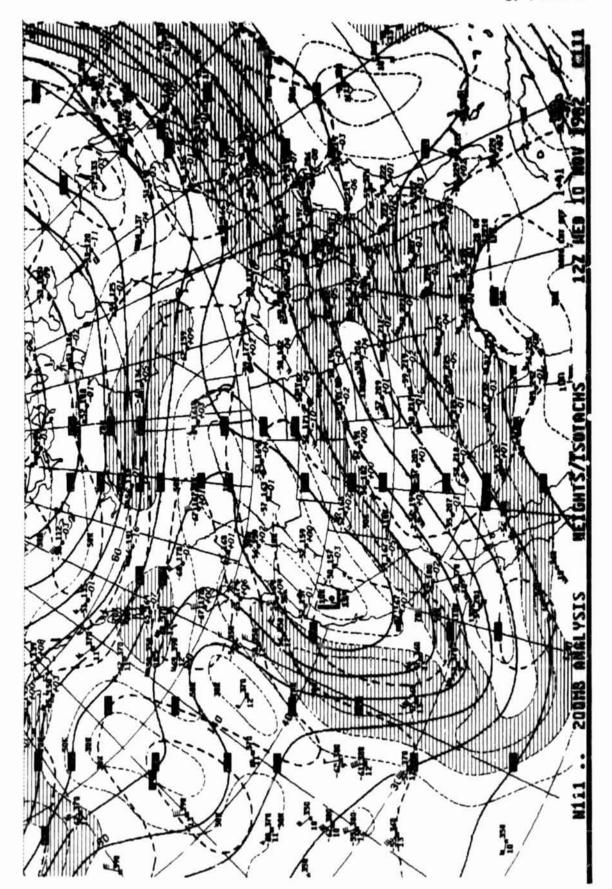


Figure A-3. 200 mb upper-air analysis for 1200 UT, 10 November 1982.

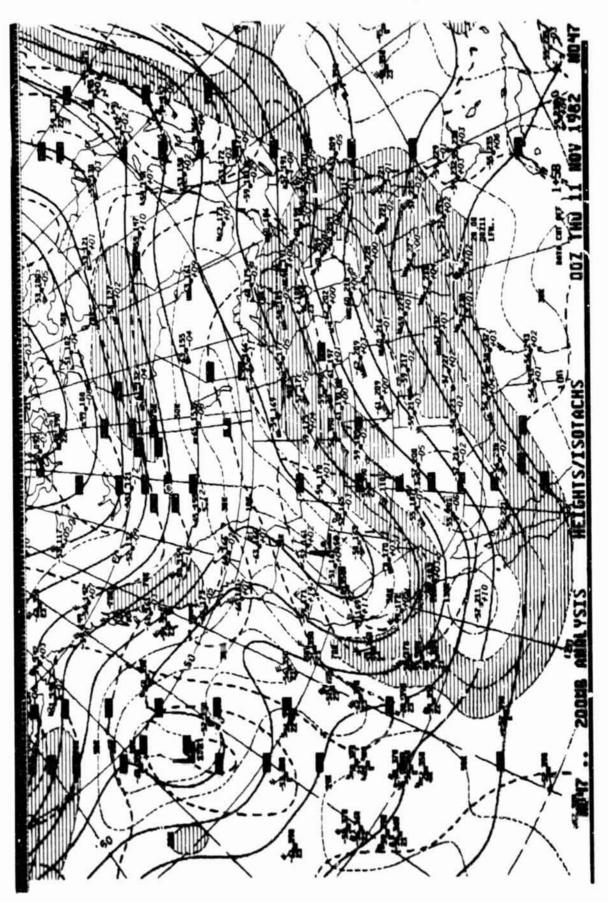


Figure A-4. 200 mb upper-air analysis for 0000 UT, 11 November 1982.

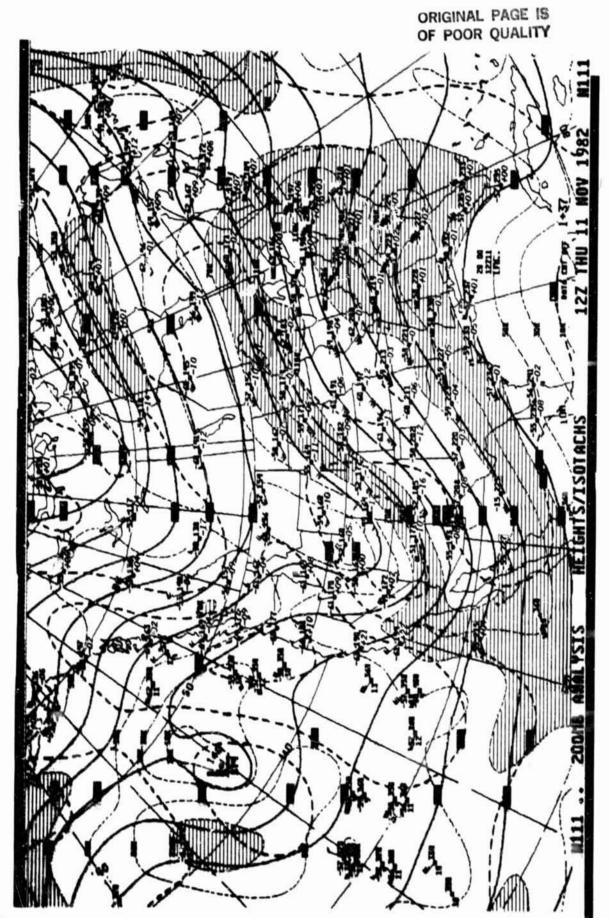


Figure A-5. 200 mb upper-air analysis for 1200 UT, 11 November 1982.

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